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**Module-6**

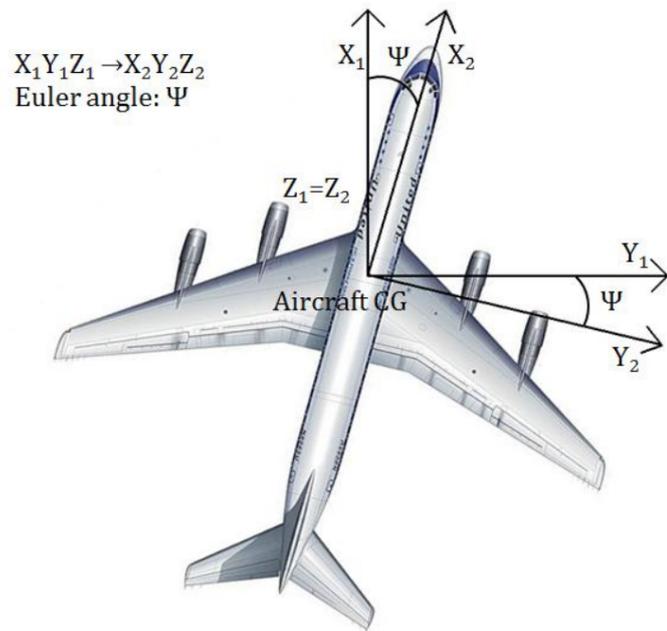
**Lecture-27**

**Euler angles & Kinematic equations**

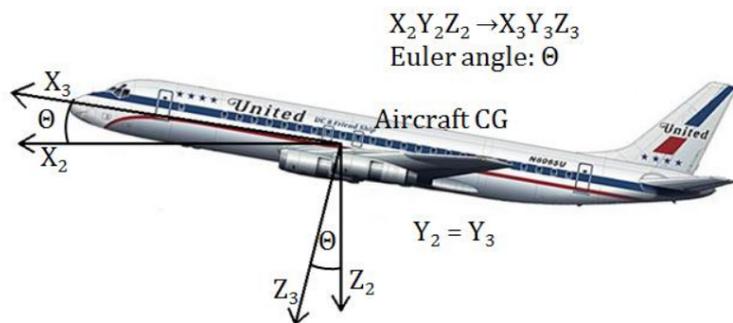
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# Euler Angles

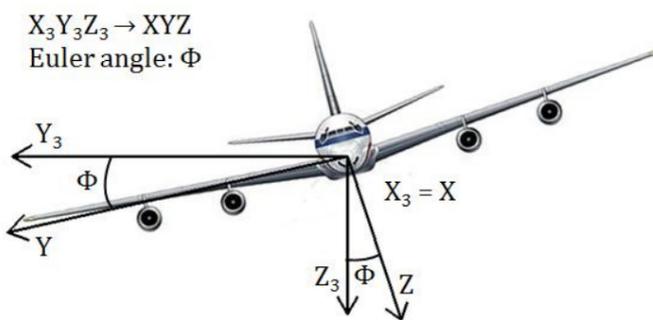
- Formulas described in previous lecture provide linear and angular velocity w.r.t.  $(X, Y, Z)$  Body fixed coordinate system.
- Now analysis of the relative motion of body fixed reference frame and inertial reference frame is required.
- There are several methods of tracking the orientation of the  $X, Y, Z$  frame with respect to earth based inertial frame  $X', Y', Z'$ .
- The most common approach is based on Euler angles.
- The introduction of Euler angle is based on a rigorous sequence that involves the introduction of a number of reference frames based on successive rotations.
  - **Step1:** Introduce a reference frame  $X_1, Y_1, Z_1$  that moves with the aircraft center of gravity while being parallel to the earth based frame  $X', Y', Z'$ .
  - **Step2:** Rotation around  $Z_1$  of an angle  $\Psi$  from the frame  $X_1, Y_1, Z_1$  to a new frame  $X_2, Y_2, Z_2$  with  $Z_1 = Z_2$ .
  - **Step3:** Rotation around  $Y_2$  of an angle  $\Theta$  from the frame  $X_2, Y_2, Z_2$  to a new frame  $X_3, Y_3, Z_3$  with  $Y_2 = Y_3$ .
  - **Step4:** Rotation around  $X_3$  of an angle  $\Phi$  from the frame  $X_3, Y_3, Z_3$  to the aircraft body frame  $X, Y, Z$  with  $X_3 = X$ .



(a)



(b)



(c)

Figure 1: Introduction of the Euler Angles  $\Psi$ ,  $\Theta$ ,  $\Phi$

## Kinematic Equations

- Angular velocities in body frame can be expressed in terms of rate of change of the Euler angles.

$$\boldsymbol{\omega} = P\hat{\mathbf{i}} + Q\hat{\mathbf{j}} + R\hat{\mathbf{k}} = \dot{\boldsymbol{\Psi}} + \dot{\boldsymbol{\Theta}} + \dot{\boldsymbol{\Phi}}$$

- Starting with the transformation  $X_1, Y_1, Z_1 \rightarrow X_2, Y_2, Z_2$ , we have  $Z_1 = Z_2$  which implies  $\hat{\mathbf{k}}_1 = \hat{\mathbf{k}}_2$ . Therefore

$$\dot{\boldsymbol{\Psi}} = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_1 = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_2$$

- Similarly, with the transformation  $X_2, Y_2, Z_2 \rightarrow X_3, Y_3, Z_3$ , we have  $Y_2 = Y_3$  which implies  $\hat{\mathbf{j}}_2 = \hat{\mathbf{j}}_3$ . Therefore

$$\dot{\boldsymbol{\Theta}} = \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_2 = \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_3$$

- Similarly, with the transformation  $X_3, Y_3, Z_3 \rightarrow X, Y, Z$ , we have  $X_3 = X$  which implies  $\hat{\mathbf{i}}_3 = \hat{\mathbf{i}}$ . Therefore

$$\dot{\boldsymbol{\Phi}} = \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}_3 = \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}$$

$$\boldsymbol{\omega} = P\hat{\mathbf{i}} + Q\hat{\mathbf{j}} + R\hat{\mathbf{k}} = \dot{\boldsymbol{\Psi}} + \dot{\boldsymbol{\Theta}} + \dot{\boldsymbol{\Phi}} = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_2 + \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_3 + \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}$$

- In transformation  $X_2, Y_2, Z_2 \rightarrow X_3, Y_3, Z_3$ ,

$$\begin{Bmatrix} U_2 \\ V_2 \\ W_2 \end{Bmatrix} = \begin{bmatrix} \cos \Theta & 0 & \sin \Theta \\ 0 & 1 & 0 \\ -\sin \Theta & 0 & \cos \Theta \end{bmatrix} \begin{Bmatrix} U_3 \\ V_3 \\ W_3 \end{Bmatrix} \quad (1)$$

$$\begin{Bmatrix} \hat{\mathbf{i}}_2 \\ \hat{\mathbf{j}}_2 \\ \hat{\mathbf{k}}_2 \end{Bmatrix} = \begin{bmatrix} \cos \Theta & 0 & \sin \Theta \\ 0 & 1 & 0 \\ -\sin \Theta & 0 & \cos \Theta \end{bmatrix} \begin{Bmatrix} \hat{\mathbf{i}}_3 \\ \hat{\mathbf{j}}_3 \\ \hat{\mathbf{k}}_3 \end{Bmatrix} \quad (2)$$

Similarly, in the transformation  $X_3, Y_3, Z_3 \rightarrow X, Y, Z$

$$\begin{Bmatrix} U_3 \\ V_3 \\ W_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi & \cos \Phi \end{bmatrix} \begin{Bmatrix} U \\ V \\ W \end{Bmatrix} \quad (3)$$

$$\begin{Bmatrix} \hat{\mathbf{i}}_3 \\ \hat{\mathbf{j}}_3 \\ \hat{\mathbf{k}}_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi & \cos \Phi \end{bmatrix} \begin{Bmatrix} \hat{\mathbf{i}} \\ \hat{\mathbf{j}} \\ \hat{\mathbf{k}} \end{Bmatrix} \quad (4)$$

- Expression for  $\hat{\mathbf{k}}_2$  in  $\hat{\mathbf{i}}, \hat{\mathbf{j}}, \hat{\mathbf{k}}$

$$\hat{\mathbf{k}}_2 = -\sin \Theta \hat{\mathbf{i}}_3 + \cos \Theta \hat{\mathbf{k}}_3 = -\sin \Theta \hat{\mathbf{i}} + \cos \Theta \hat{\mathbf{k}}_3$$

where,  $\hat{\mathbf{k}}_3 = \sin \Phi \hat{\mathbf{j}} + \cos \Phi \hat{\mathbf{k}}$ , so

$$\hat{\mathbf{k}}_2 = -\sin \Theta \hat{\mathbf{i}} + \cos \Theta \sin \Phi \hat{\mathbf{j}} + \cos \Theta \cos \Phi \hat{\mathbf{k}}$$

Similarly, Expression for  $\hat{\mathbf{j}}_3$  in  $\hat{\mathbf{i}}, \hat{\mathbf{j}}, \hat{\mathbf{k}}$

$$\hat{\mathbf{j}}_3 = \cos \Phi \hat{\mathbf{j}} - \sin \Phi \hat{\mathbf{k}}$$

- Now using

$$\boldsymbol{\omega} = P\hat{\mathbf{i}} + Q\hat{\mathbf{j}} + R\hat{\mathbf{k}} = \dot{\Psi} + \dot{\Theta} + \dot{\Phi} = \dot{\Psi}\hat{\mathbf{k}}_2 + \dot{\Theta}\hat{\mathbf{j}}_3 + \dot{\Phi}\hat{\mathbf{i}}$$

we have

$$= \dot{\Psi}\hat{\mathbf{k}}_2(-\sin \Theta \hat{\mathbf{i}}_3 + \cos \Theta \sin \Phi \hat{\mathbf{j}} + \cos \Theta \cos \Phi \hat{\mathbf{k}}) + \dot{\Theta}(\cos \Phi \hat{\mathbf{j}} - \sin \Phi \hat{\mathbf{k}}) + \dot{\Phi}\hat{\mathbf{i}}$$

$$P = \dot{\Phi} - \sin \Theta \dot{\Psi}$$

$$Q = \cos \Phi \dot{\Theta} + \cos \Theta \sin \Phi \dot{\Psi}$$

$$R = \cos \Theta \cos \Phi \dot{\Psi} - \sin \Phi \dot{\Theta}$$

- Rearranging in matrix form

$$\begin{Bmatrix} P \\ Q \\ R \end{Bmatrix} = \begin{bmatrix} 1 & 0 & -\sin \Theta \\ 0 & \cos \Phi & \cos \Theta \sin \Phi \\ 0 & -\sin \Phi & \cos \Theta \cos \Phi \end{bmatrix} \begin{Bmatrix} \dot{\Phi} \\ \dot{\Theta} \\ \dot{\Psi} \end{Bmatrix}$$

or,

$$\begin{Bmatrix} \dot{\Phi} \\ \dot{\Theta} \\ \dot{\Psi} \end{Bmatrix} = \begin{bmatrix} 1 & \sin \Phi \tan \Theta & \cos \Phi \tan \Theta \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi \sec \Theta & \cos \Phi \sec \Theta \end{bmatrix} \begin{Bmatrix} P \\ Q \\ R \end{Bmatrix}$$

**Note:**

*There is a singularity associated with  $\Theta = 90^\circ$ . This is one of the reason for using quaternion for large-scale simulation*