
Module-5

Lecture-24

Lateral Stability and Control

Lateral stability

An airplane is said to have roll (lateral) stability, if a restoring moment is generated when it is disturbed in bank orientation (ϕ).

- The restoring moment is function of side slip angle, β .
- The requirement for roll stability is that $C_{l_\beta} < 0$.
- The rolling moment created in airplane due to side slip angle also depends on
 - Wing dihedral
 - Wing sweep
 - Position of wing and fuselage
 - Vertical tail
- The major contributor to C_{l_β} is the wing dihedral angle, Γ .
- When an aircraft is disturbed from a wing-level attitude, it will begin to side slip.

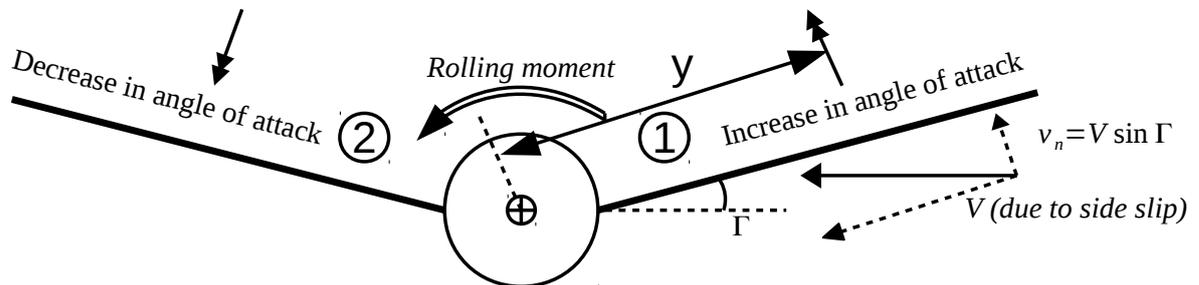


Figure 1: Wing-body dihedral effect

On wing 1,

$$\begin{aligned} \Delta\alpha &= \frac{v_n}{u} \\ &= \frac{V \sin \Gamma}{u} \\ \beta &\cong \frac{v}{u} \\ \Delta\alpha &= \beta\Gamma \end{aligned}$$

On wing 2, angle of attack will decrease. Resulting in negative rolling moment to positive side slip angle.

$$C_{l_\beta} < 0$$

Rolling moment due to right wing

$$L_{w,R} = -\frac{1}{2}\rho V^2 C_{L_{\alpha,w}} \Delta\alpha \int_0^{\frac{b}{2}} c(y) \cdot y \cdot dy$$

Rolling moment due to left wing

$$L_{w,L} = -\frac{1}{2}\rho V^2 C_{L_{\alpha,w}} \Delta\alpha \int_{-\frac{b}{2}}^0 c(y) \cdot y \cdot dy$$

Rolling moment (total)

$$L_w = -2\frac{1}{2}\rho V^2 C_{L_{\alpha,w}} \Delta\alpha \int_0^{\frac{b}{2}} cy dy$$

$$\because \Delta\alpha = \beta\Gamma \text{ and } \bar{y} = \frac{2}{S_w} \int_0^{\frac{b}{2}} cy dy$$

$$L_w = -2\frac{1}{2}\rho V^2 C_{L_{\alpha,w}} \Gamma \beta \frac{S}{2} \bar{y}$$

$$(C_{l,w})_{\Gamma} = \frac{L_w}{\frac{1}{2}\rho V^2 S b} = -\Gamma \beta C_{L_{\alpha,w}} \frac{\bar{y}}{b}$$

$$C_{l_{\beta}} = -\Gamma C_{L_{\alpha}} \frac{\bar{y}}{b}$$

$C_{l_{\beta,w}} < 0$, Stabilizing for $\Gamma > 0$: Dihedral

$C_{l_{\beta,w}} > 0$, Destabilizing for $\Gamma < 0$: Anhedral

- $C_{l_{\beta}}$: Due to wing sweep

$$(L_w)_{R,\Lambda} = -C_L \frac{S}{2} \frac{1}{2} \rho V^2 \bar{y} \cos^2(\Lambda - \beta)$$

$$(L_w)_{L,\Lambda} = C_L \frac{S}{2} \frac{1}{2} \rho V^2 \bar{y} \cos^2(\Lambda + \beta)$$

Hence,

$$(L_w)_{\Lambda,Total} = -C_L \frac{S}{2} \frac{1}{2} \rho V^2 \bar{y} \{ \cos^2(\Lambda - \beta) - \cos^2(\Lambda + \beta) \}$$

\bar{y} is the location of resultant lift on the wing half

Assume β to be small; $\cos \beta \rightarrow 1$ and $\sin \beta \rightarrow \beta$

$$(L_w)_{\Gamma,Total} = -C_L \frac{1}{2} \rho V_{\infty}^2 \bar{y} \beta \cdot \sin 2\Gamma$$

$$(C_{l_w})_{\Gamma} = -C_L \frac{\bar{y}}{b} \beta \sin 2\Gamma$$

$$C_{l_{\beta}} = -C_L \frac{\bar{y}}{b} \sin 2\Gamma$$

$C_{l_{\beta}} < 0 \Rightarrow$ Stabilizing

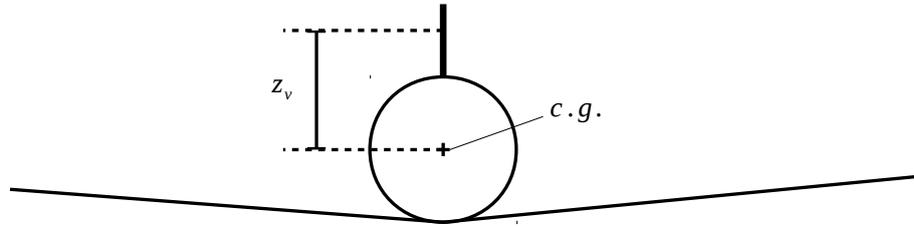


Figure 2: Effect of vertical tail on lateral stability

- C_{l_β} : Due to vertical tail

The rolling moment due to vertical tail when aircraft is side slipping can be written as

$$l = -\frac{1}{2}\rho V^2 \eta_v S_v \left(\frac{dC_L}{d\alpha} \right)_v \beta \cdot z_v$$

hence,

$$(C_{l_\beta})_v = -\eta_v \frac{S_v}{S_w} \frac{z_v}{b} C_{L_{\alpha,v}}$$

Roll control

- It is achieved by differential deflection of small flaps called ailerons.
- The basic principle lies on the fact that due to differential deflection of ailerons, the lift distribution over the wing becomes unequal, causing a rolling moment.
- An approximate expression for roll control power can be obtained using simple strip integration method.

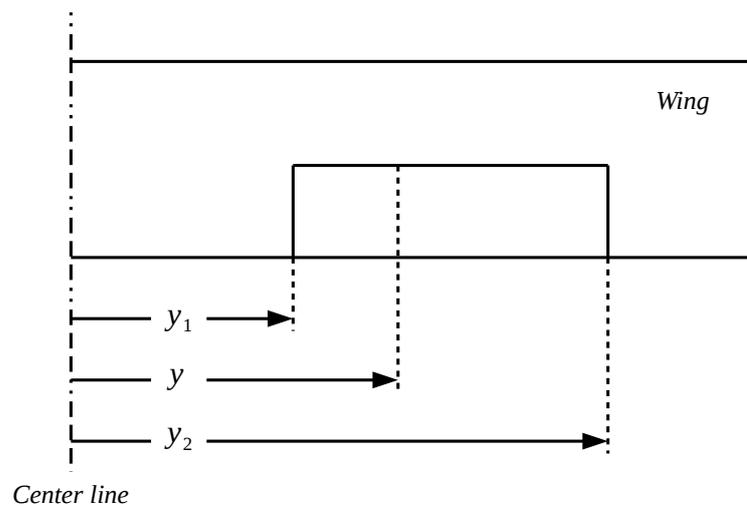


Figure 3: Aileron element for integration

$$\Delta(\text{Rolling moment due to } \delta a) = \Delta l$$

$$\begin{aligned}
&= (\Delta \text{Lift}) \cdot y \\
\Delta C_l &= \frac{\Delta L}{qSb} = \frac{C_l Q c y dy}{Q S b} = \frac{C_l c y dy}{S b} \\
C_l &= C_{L_\alpha} \cdot \frac{d\alpha}{d\delta a} \cdot \delta a = C_{L_\alpha} \cdot \tau \cdot \delta a
\end{aligned}$$

Integrating over the region containing the aileron yields

$$\begin{aligned}
C_l &= \frac{2C_{L_{\alpha,w}} \tau \delta a}{Sb} \int_{y_1}^{y_2} c y dy \\
C_{l_{\delta a}} &= \frac{2C_{L_{\alpha,w}} \tau}{Sb} \int_{y_1}^{y_2} c y dy
\end{aligned}$$