
Module-6

Lecture-27

Euler angles & Kinematic equations

Euler Angles

- Formulas described in previous lecture provide linear and angular velocity w.r.t. (X, Y, Z) Body fixed coordinate system.
- Now analysis of the relative motion of body fixed reference frame and inertial reference frame is required.
- There are several methods of tracking the orientation of the X, Y, Z frame with respect to earth based inertial frame X', Y', Z' .
- The most common approach is based on Euler angles.
- The introduction of Euler angle is based on a rigorous sequence that involves the introduction of a number of reference frames based on successive rotations.
 - **Step1:** Introduce a reference frame X_1, Y_1, Z_1 that moves with the aircraft center of gravity while being parallel to the earth based frame X', Y', Z' .
 - **Step2:** Rotation around Z_1 of an angle Ψ from the frame X_1, Y_1, Z_1 to a new frame X_2, Y_2, Z_2 with $Z_1 = Z_2$.
 - **Step3:** Rotation around Y_2 of an angle Θ from the frame X_2, Y_2, Z_2 to a new frame X_3, Y_3, Z_3 with $Y_2 = Y_3$.
 - **Step4:** Rotation around X_3 of an angle Φ from the frame X_3, Y_3, Z_3 to the aircraft body frame X, Y, Z with $X_3 = X$.

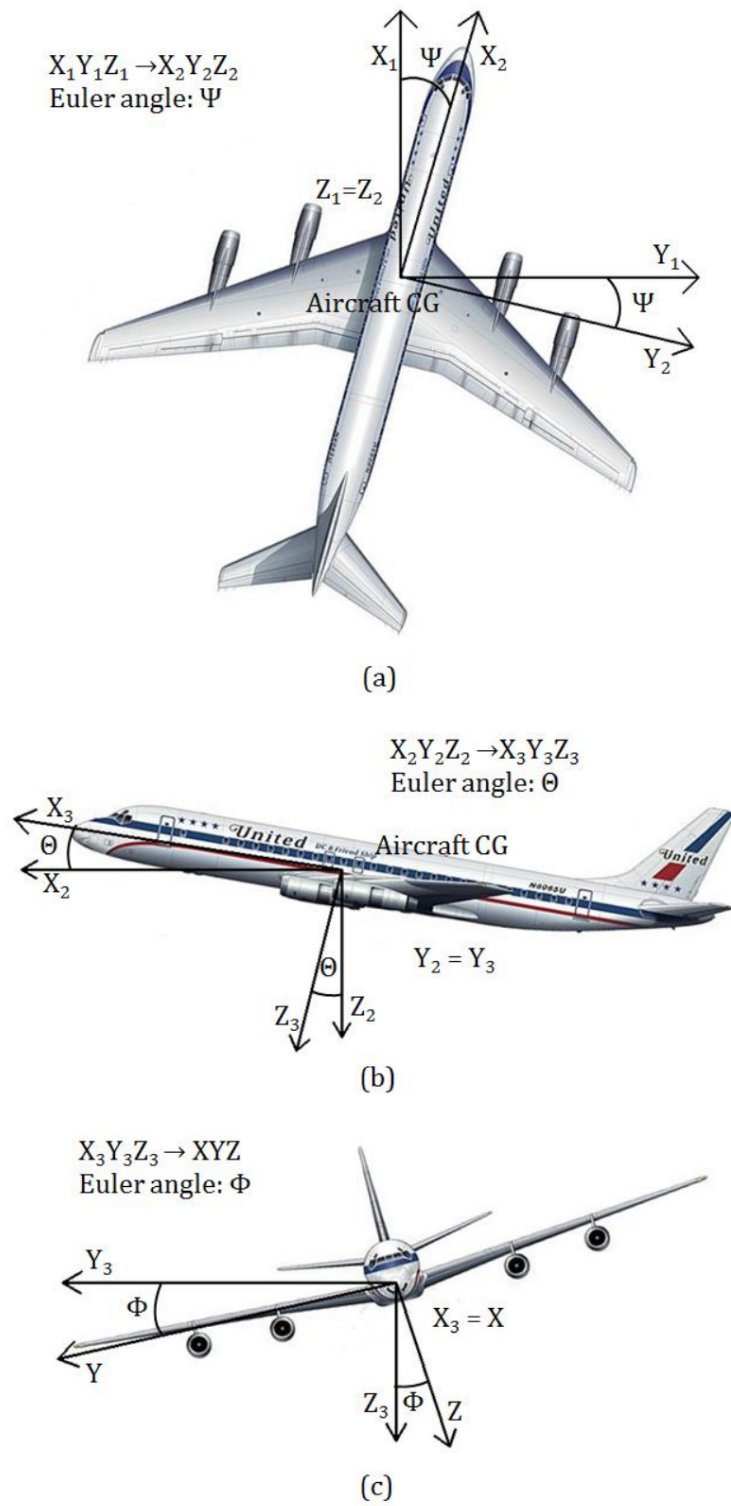


Figure 1: Introduction of the Euler Angles Ψ , Θ , Φ

Kinematic Equations

- Angular velocities in body frame can be expressed in terms of rate of change of the Euler angles.

$$\boldsymbol{\omega} = P\hat{\mathbf{i}} + Q\hat{\mathbf{j}} + R\hat{\mathbf{k}} = \dot{\boldsymbol{\Psi}} + \dot{\boldsymbol{\Theta}} + \dot{\boldsymbol{\Phi}}$$

- Starting with the transformation $X_1, Y_1, Z_1 \rightarrow X_2, Y_2, Z_2$, we have $Z_1 = Z_2$ which implies $\hat{\mathbf{k}}_1 = \hat{\mathbf{k}}_2$. Therefore

$$\dot{\boldsymbol{\Psi}} = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_1 = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_2$$

- Similarly, with the transformation $X_2, Y_2, Z_2 \rightarrow X_3, Y_3, Z_3$, we have $Y_2 = Y_3$ which implies $\hat{\mathbf{j}}_2 = \hat{\mathbf{j}}_3$. Therefore

$$\dot{\boldsymbol{\Theta}} = \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_2 = \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_3$$

- Similarly, with the transformation $X_3, Y_3, Z_3 \rightarrow X, Y, Z$, we have $X_3 = X$ which implies $\hat{\mathbf{i}}_3 = \hat{\mathbf{i}}$. Therefore

$$\dot{\boldsymbol{\Phi}} = \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}_3 = \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}$$

$$\boldsymbol{\omega} = P\hat{\mathbf{i}} + Q\hat{\mathbf{j}} + R\hat{\mathbf{k}} = \dot{\boldsymbol{\Psi}} + \dot{\boldsymbol{\Theta}} + \dot{\boldsymbol{\Phi}} = \dot{\boldsymbol{\Psi}}\hat{\mathbf{k}}_2 + \dot{\boldsymbol{\Theta}}\hat{\mathbf{j}}_3 + \dot{\boldsymbol{\Phi}}\hat{\mathbf{i}}$$

- In transformation $X_2, Y_2, Z_2 \rightarrow X_3, Y_3, Z_3$,

$$\begin{Bmatrix} U_2 \\ V_2 \\ W_2 \end{Bmatrix} = \begin{bmatrix} \cos \Theta & 0 & \sin \Theta \\ 0 & 1 & 0 \\ -\sin \Theta & 0 & \cos \Theta \end{bmatrix} \begin{Bmatrix} U_3 \\ V_3 \\ W_3 \end{Bmatrix} \quad (1)$$

$$\begin{Bmatrix} \hat{\mathbf{i}}_2 \\ \hat{\mathbf{j}}_2 \\ \hat{\mathbf{k}}_2 \end{Bmatrix} = \begin{bmatrix} \cos \Theta & 0 & \sin \Theta \\ 0 & 1 & 0 \\ -\sin \Theta & 0 & \cos \Theta \end{bmatrix} \begin{Bmatrix} \hat{\mathbf{i}}_3 \\ \hat{\mathbf{j}}_3 \\ \hat{\mathbf{k}}_3 \end{Bmatrix} \quad (2)$$

Similarly, in the transformation $X_3, Y_3, Z_3 \rightarrow X, Y, Z$

$$\begin{Bmatrix} U_3 \\ V_3 \\ W_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi & \cos \Phi \end{bmatrix} \begin{Bmatrix} U \\ V \\ W \end{Bmatrix} \quad (3)$$

$$\begin{Bmatrix} \hat{\mathbf{i}}_3 \\ \hat{\mathbf{j}}_3 \\ \hat{\mathbf{k}}_3 \end{Bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi & \cos \Phi \end{bmatrix} \begin{Bmatrix} \hat{\mathbf{i}} \\ \hat{\mathbf{j}} \\ \hat{\mathbf{k}} \end{Bmatrix} \quad (4)$$

- Expression for \hat{k}_2 in $\hat{i}, \hat{j}, \hat{k}$

$$\hat{k}_2 = -\sin \Theta \hat{i}_3 + \cos \Theta \hat{k}_3 = -\sin \Theta \hat{i} + \cos \Theta \hat{k}_3$$

where, $\hat{k}_3 = \sin \Phi \hat{j} + \cos \Phi \hat{k}$, so

$$\hat{k}_2 = -\sin \Theta \hat{i} + \cos \Theta \sin \Phi \hat{j} + \cos \Theta \cos \Phi \hat{k}$$

Similarly, Expression for \hat{j}_3 in $\hat{i}, \hat{j}, \hat{k}$

$$\hat{j}_3 = \cos \Phi \hat{j} - \sin \Phi \hat{k}$$

- Now using

$$\omega = P\hat{i} + Q\hat{j} + R\hat{k} = \dot{\Psi} + \dot{\Theta} + \dot{\Phi} = \dot{\Psi}\hat{k}_2 + \dot{\Theta}\hat{j}_3 + \dot{\Phi}\hat{i}$$

we have

$$= \dot{\Psi}\hat{k}_2(-\sin \Theta \hat{i}_3 + \cos \Theta \sin \Phi \hat{j} + \cos \Theta \cos \Phi \hat{k}) + \dot{\Theta}(\cos \Phi \hat{j} - \sin \Phi \hat{k}) + \dot{\Phi}\hat{i}$$

$$\begin{aligned} P &= \dot{\Phi} - \sin \Theta \dot{\Psi} \\ Q &= \cos \Phi \dot{\Theta} + \cos \Theta \sin \Phi \dot{\Psi} \\ R &= \cos \Theta \cos \Phi \dot{\Psi} - \sin \Phi \dot{\Theta} \end{aligned}$$

- Rearranging in matrix form

$$\begin{Bmatrix} P \\ Q \\ R \end{Bmatrix} = \begin{bmatrix} 1 & 0 & -\sin \Theta \\ 0 & \cos \Phi & \cos \Theta \sin \Phi \\ 0 & -\sin \Phi & \cos \Theta \cos \Phi \end{bmatrix} \begin{Bmatrix} \dot{\Phi} \\ \dot{\Theta} \\ \dot{\Psi} \end{Bmatrix}$$

or,

$$\begin{Bmatrix} \dot{\Phi} \\ \dot{\Theta} \\ \dot{\Psi} \end{Bmatrix} = \begin{bmatrix} 1 & \sin \Phi \tan \Theta & \cos \Phi \tan \Theta \\ 0 & \cos \Phi & -\sin \Phi \\ 0 & \sin \Phi \sec \Theta & \cos \Phi \sec \Theta \end{bmatrix} \begin{Bmatrix} P \\ Q \\ R \end{Bmatrix}$$

Note:

There is a singularity associated with $\Theta = 90^\circ$. This is one of the reason for using quaternion for large-scale simulation