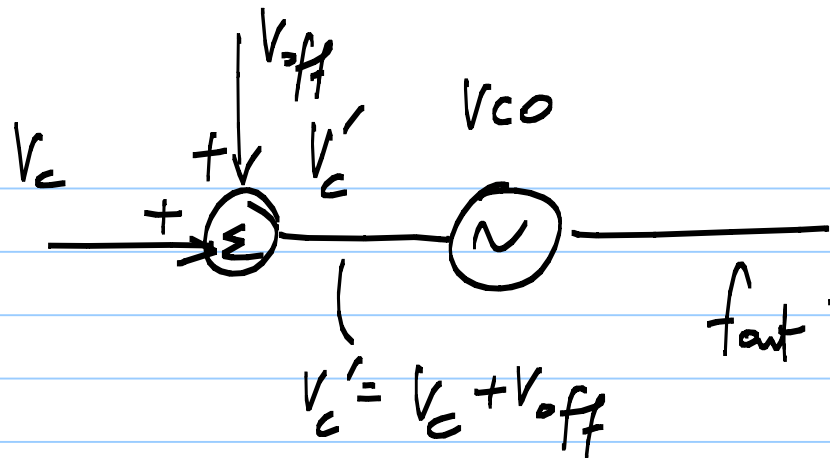


Lecture 48:

* Reference feedthrough due to periodic error of the phase detector

* $e(t) = 0$ if $\Delta\Phi = \Phi_{ref} - \Phi_{out}/N = 0$

if the output frequency equals the free running frequency of the VCO.

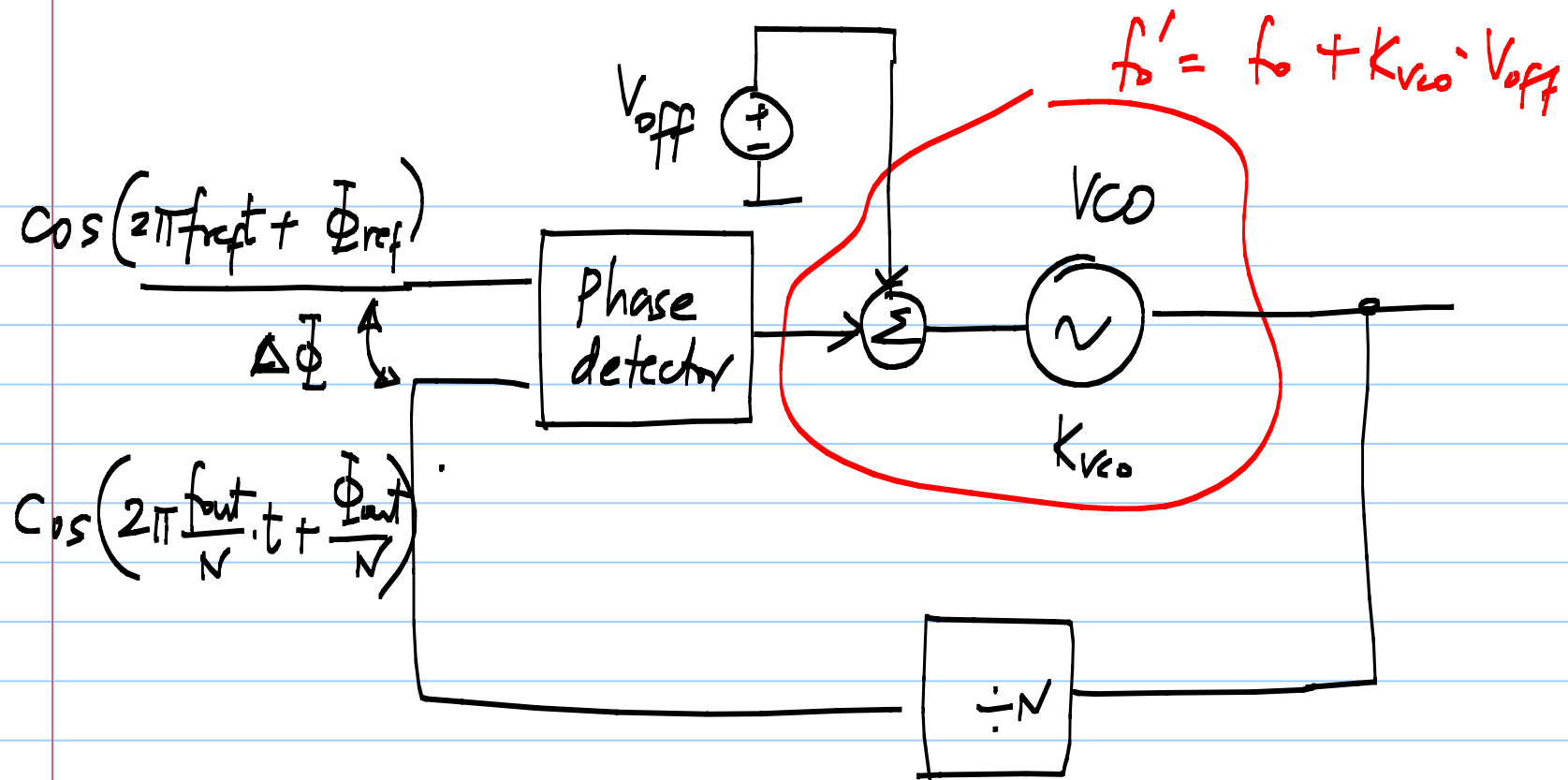


$$f_{out} = f_0 + K_{VCO} \cdot V_c'$$

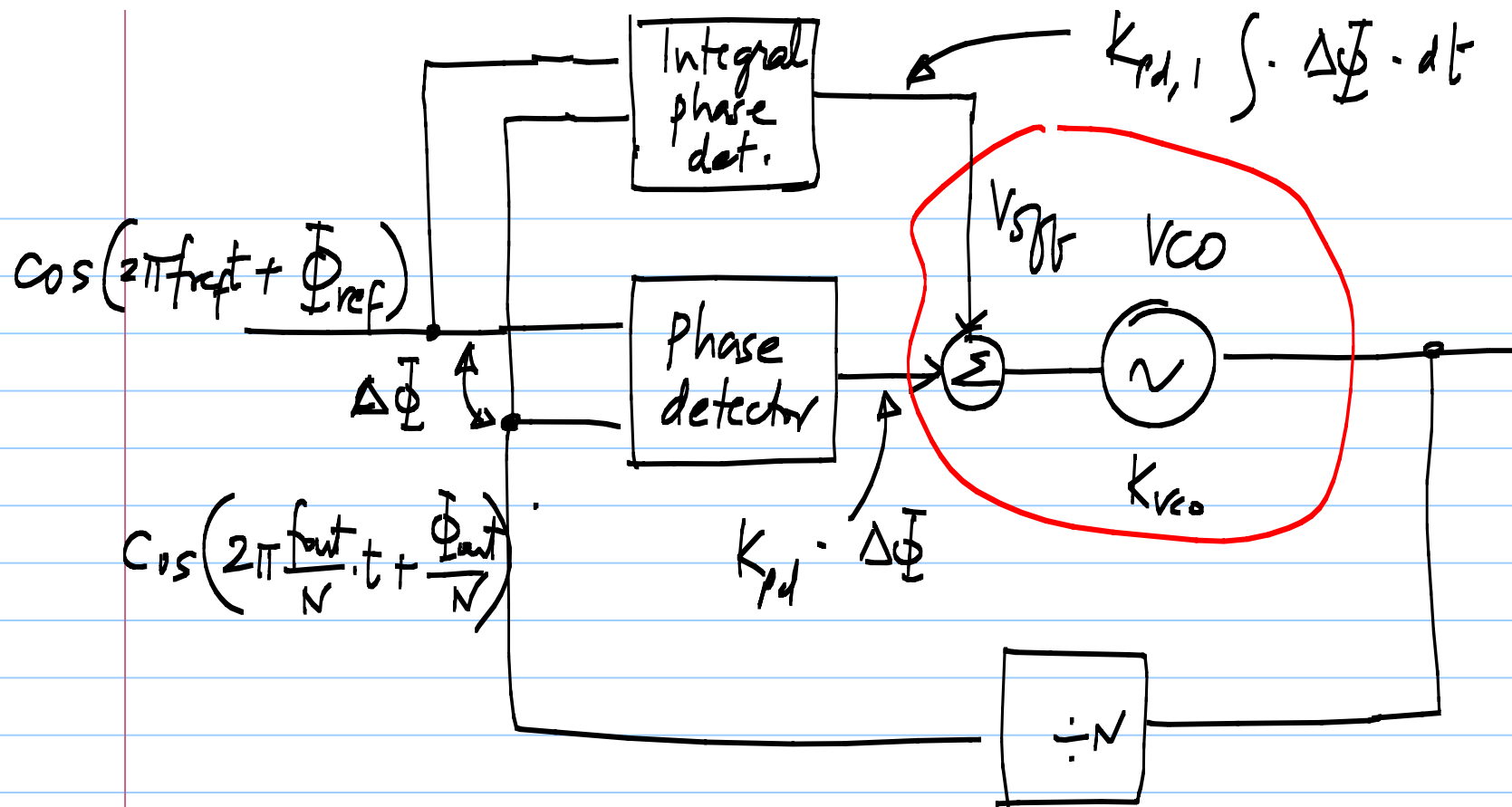
$$V_c' = V_c + V_{off}$$

$$f' = \underline{f_0 + K_{VCO} \cdot V_{off}}$$

$$= \underbrace{(f_0 + K_{VCO} \cdot V_{off})}_{\text{free running frequency}} + \underbrace{K_{VCO} V_c}$$



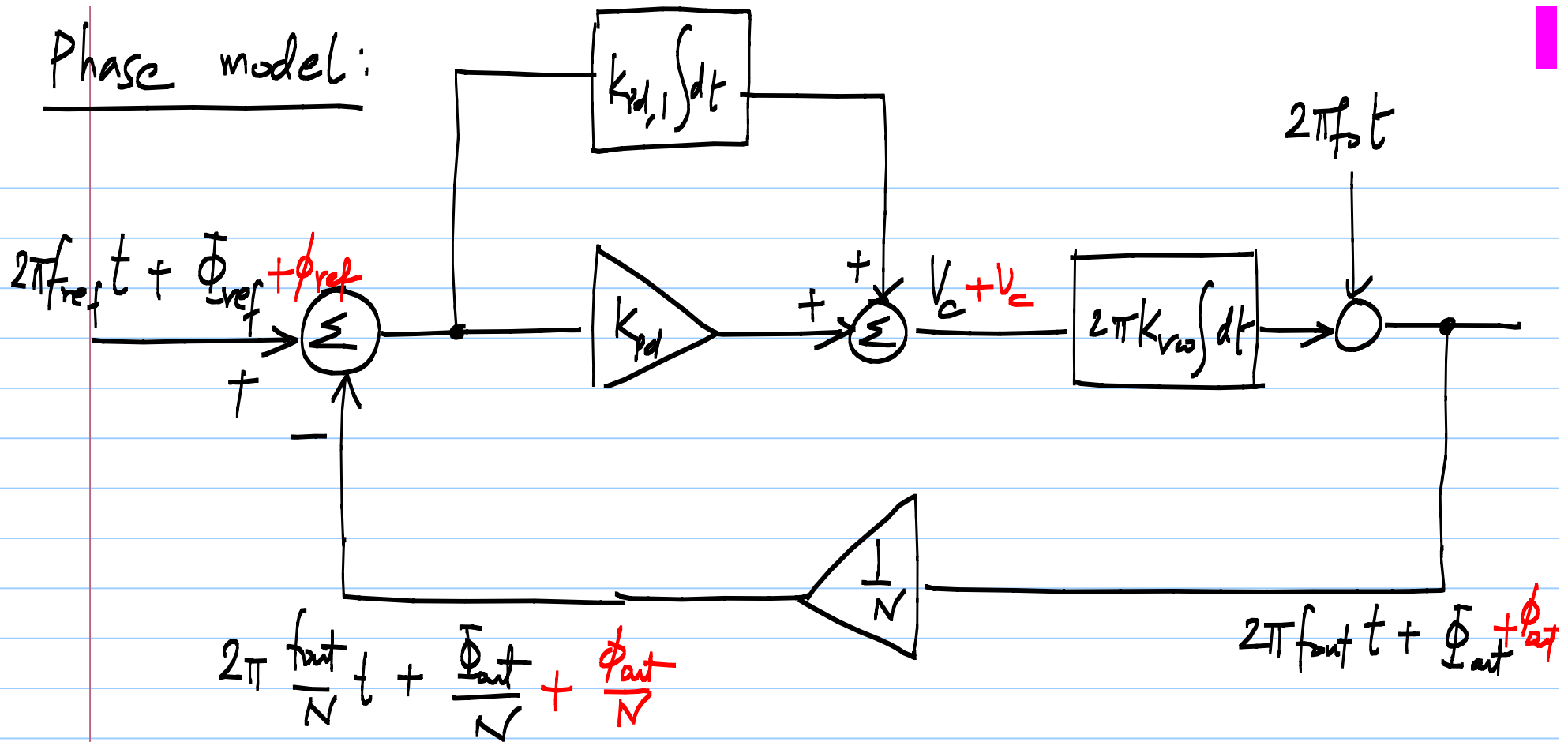
* Adjust V_{eff} continuously until f'_0 becomes equal to $N f_{ref}$

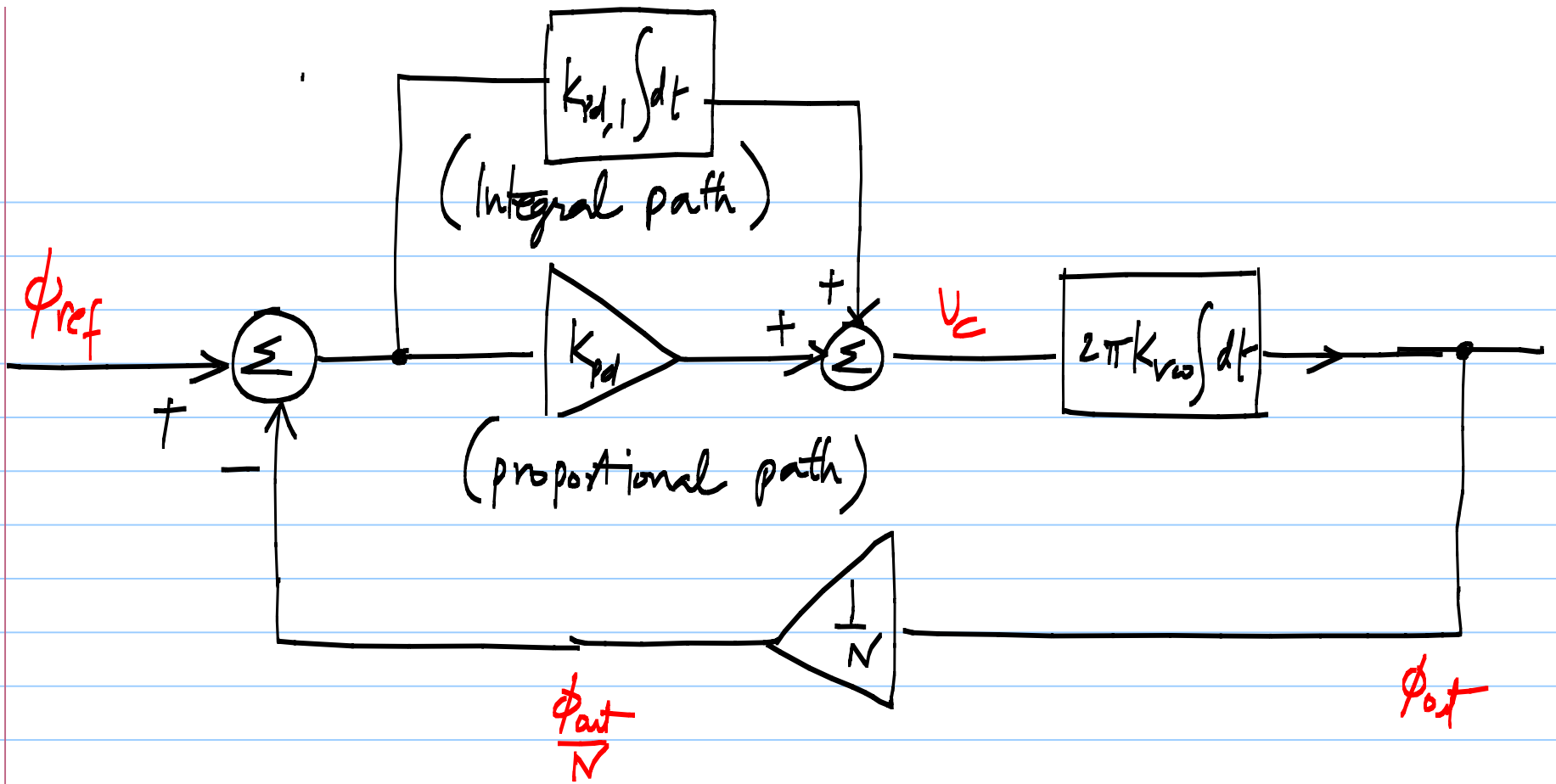


* Integrate $\Phi_{ref} - \frac{\Phi_{out}}{N}$ (slowly) and drive V_{ctrl} .

* $\Phi_{ref} - \frac{\Phi_{out}}{N} = 0$ in steady state; No ref. feed through.

Phase model:





* Type II phase locked loop.

Type II phase locked loop:

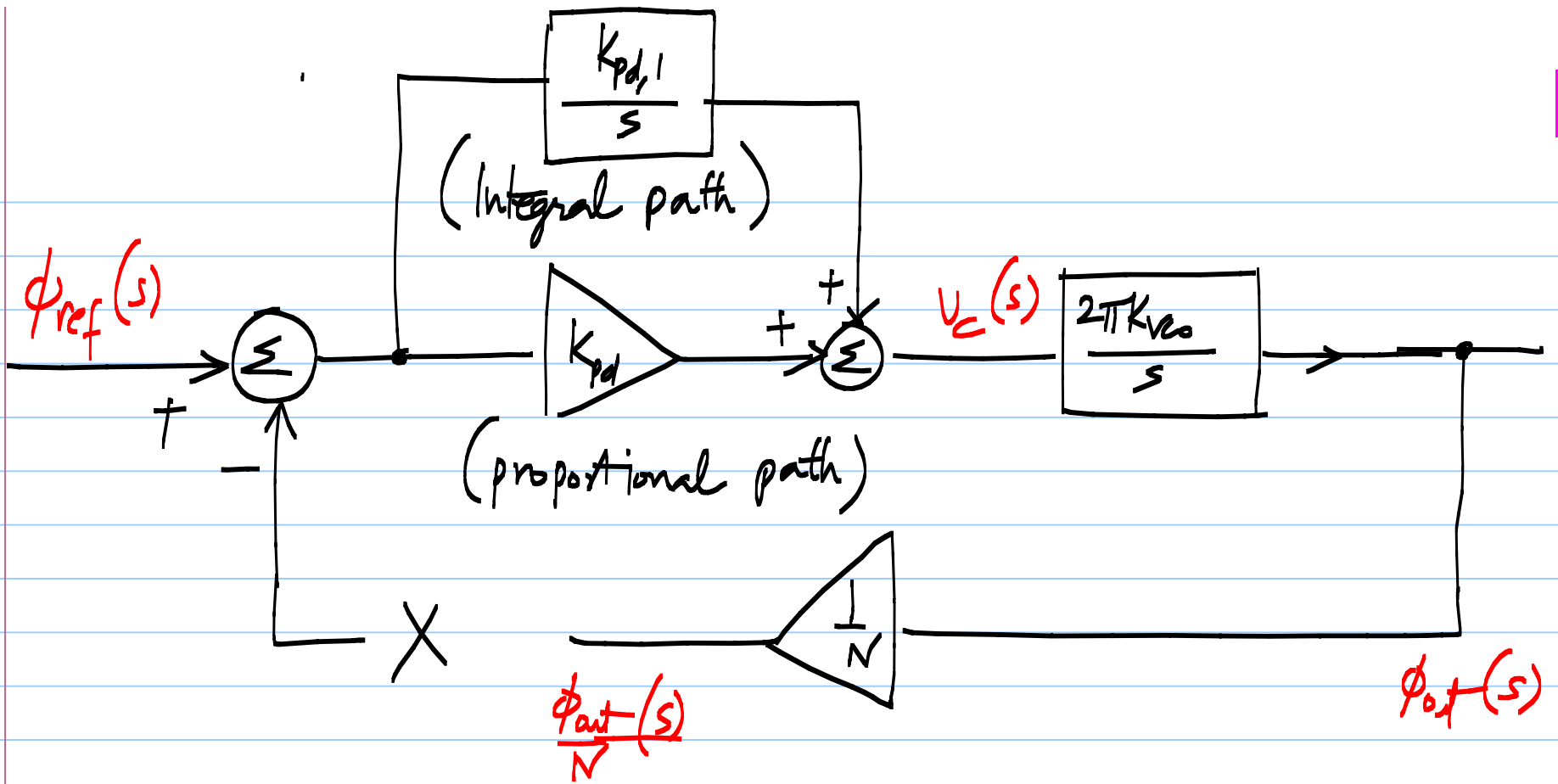
* operating point: $\Phi_{ref} - \Phi_{out}/N = 0$

$$f_{out} = N f_{ref}$$
$$V_c = \frac{f_{out} - f_0}{K_{VCO}} = \frac{N f_{ref} - f_0}{K_{VCO}}$$

Integral phase detector

* Periodic error $e(t) = 0 \Rightarrow$ No reference spurs

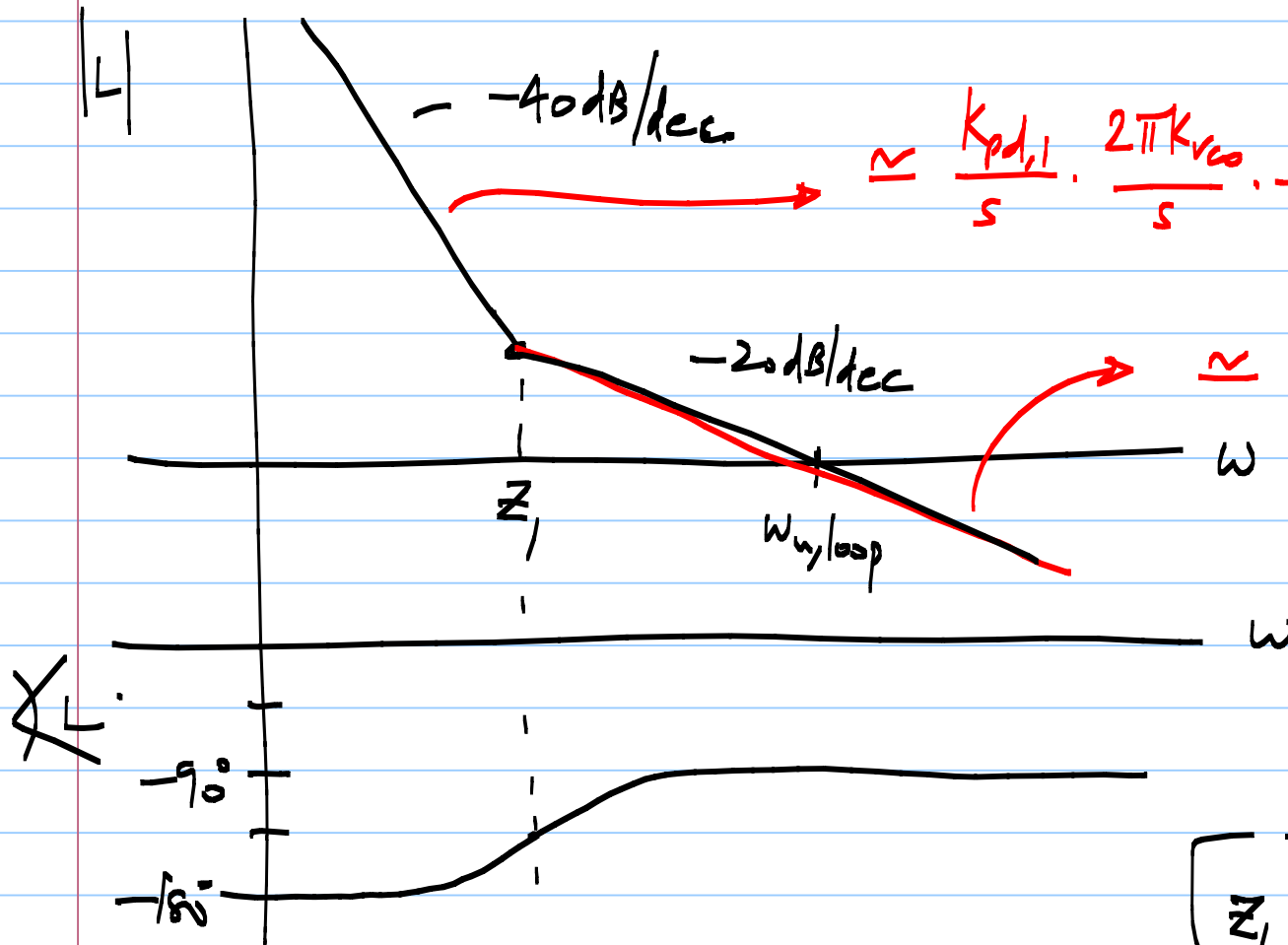
* Lock range limited by VCO range.



$$L(s) = \left(\frac{K_{pd,1}}{s} + K_{pd} \right) \cdot \frac{2\pi K_{vco}}{s} \cdot \frac{1}{N}$$

$$L(s) = \left(\frac{K_{pd1}}{s} + K_{pd} \right) \cdot \frac{2\pi K_{vco}}{s} \cdot \frac{1}{N}$$

* Two poles at the origin



$$\approx \frac{K_{pd1}}{s} \cdot \frac{2\pi K_{vco}}{s} \cdot \frac{1}{N}$$

* One zero at $\frac{K_{pd1}}{K_{pd}}$

$$\approx K_{pd} \cdot \frac{2\pi K_{vco}}{s} \cdot \frac{1}{N}$$

$$\omega_{BW} = \omega_{u,loop}$$

$$= \frac{2\pi K_{vco} \cdot K_{pd}}{N \cdot s}$$

$$z_1 < \omega_{BW}$$

$$L(s) = \left(\frac{K_{pd,1}}{s} + K_{pd} \right) \cdot \frac{2\pi K_{vco}}{N \cdot s} = \frac{2\pi K_{vco} \cdot K_{pd,1}}{N \cdot s^2} \left(1 + s \frac{K_{pd}}{K_{pd,1}} \right)$$

$$\frac{\phi_{out}(s)}{\phi_{ref}(s)} = N \cdot \frac{1}{1 + \frac{1}{L}} = \frac{N}{1 + \frac{N \cdot s^2}{2\pi K_{vco} K_{pd,1} \left(1 + s \frac{K_{pd}}{K_{pd,1}} \right)}}$$

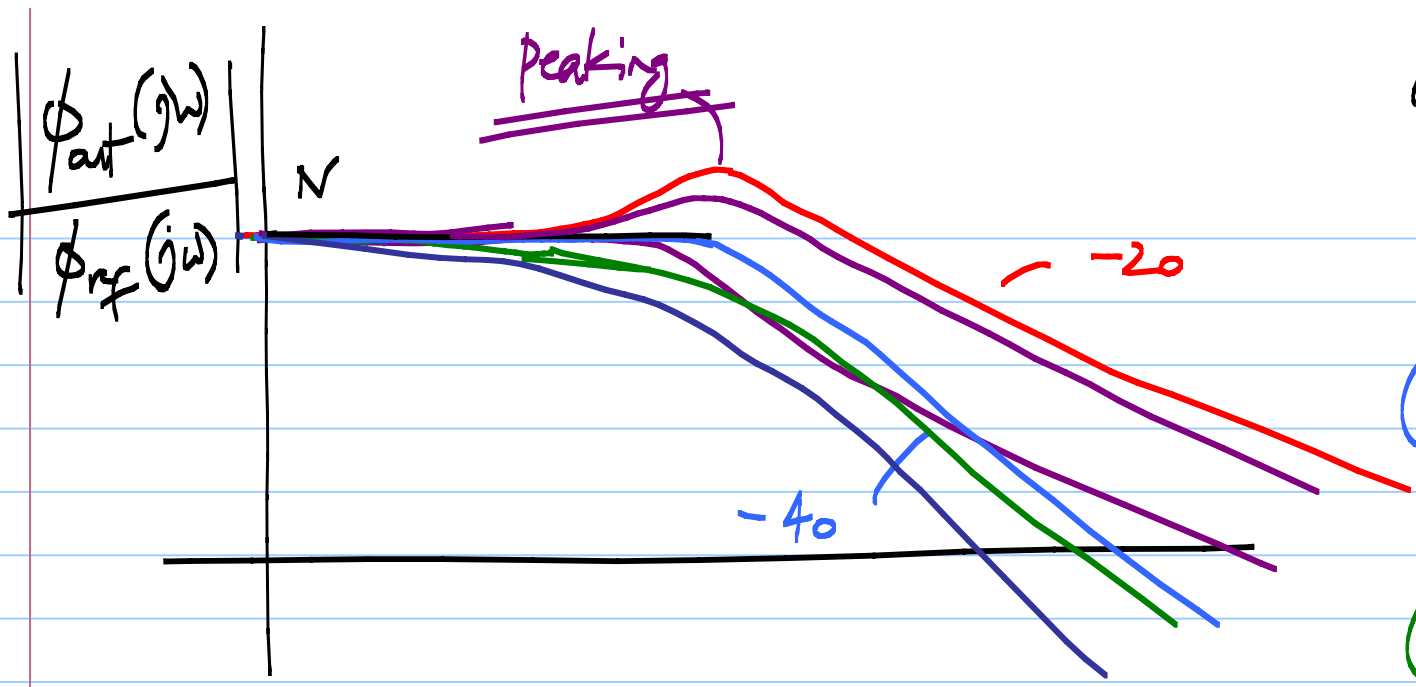
$$= N \cdot \frac{1 + s \frac{K_{pd}}{K_{pd,1}}}{1 + s \frac{K_{pd}}{K_{pd,1}} + \frac{N \cdot s^2}{2\pi K_{vco} K_{pd,1}}}$$

$$z_1 = \frac{K_{pd,1}}{K_{pd}} \quad ; \quad \omega_{n,loop} = \frac{2\pi K_{vco} K_{pd}}{N}$$

$$\frac{\phi_{out}(s)}{\phi_{ref}(s)} = N_o \frac{1 + \frac{s}{z_1}}{1 + \frac{s}{z_1} + \frac{s^2}{z_1 \cdot \omega_{n,loop}}}$$

$$\omega_n = \sqrt{\omega_{n,loop} \cdot z_1}$$

$$\zeta = \frac{\omega_{n,loop}}{2\sqrt{\omega_{n,loop} z_1}} = \frac{1}{2} \sqrt{\frac{\omega_{n,loop}}{z_1}}$$



dc gain = N

$\xi = \frac{1}{\sqrt{2}}$
(maximally flat)

$\xi = 1$
(critical damping)

$\xi = 10$
(limited peaking)

$$\frac{\phi_{out}}{\phi_{ref}} = \frac{N}{1 + \frac{s}{z_1} + \frac{s^2}{\omega_{nloop} z_1}} \cdot \left(1 + \frac{s}{z_1}\right)$$

$$\frac{\phi_{ref}(s)}{\phi_{out}(s)} = N \cdot \frac{1 + s/z_1}{1 + \frac{s}{z_1} + \frac{s^2}{z_1 \cdot \omega_{n,loop}}}$$

$$z_1 = \frac{K_{pd,1}}{K_{pd}}$$

$$\omega_{n,loop} = \frac{2\pi K_{vco} K_{pd}}{N}$$

* $\xi = 1$: critical damping,

$$\xi = \frac{1}{2} \sqrt{\frac{\omega_{n,loop}}{z_1}}$$

result in magnitude response peaking $\omega_p = \sqrt{\omega_{n,loop} \cdot z_1}$
because of the zero

* $\xi \gg 1$: Limit the peaking, but slower response.

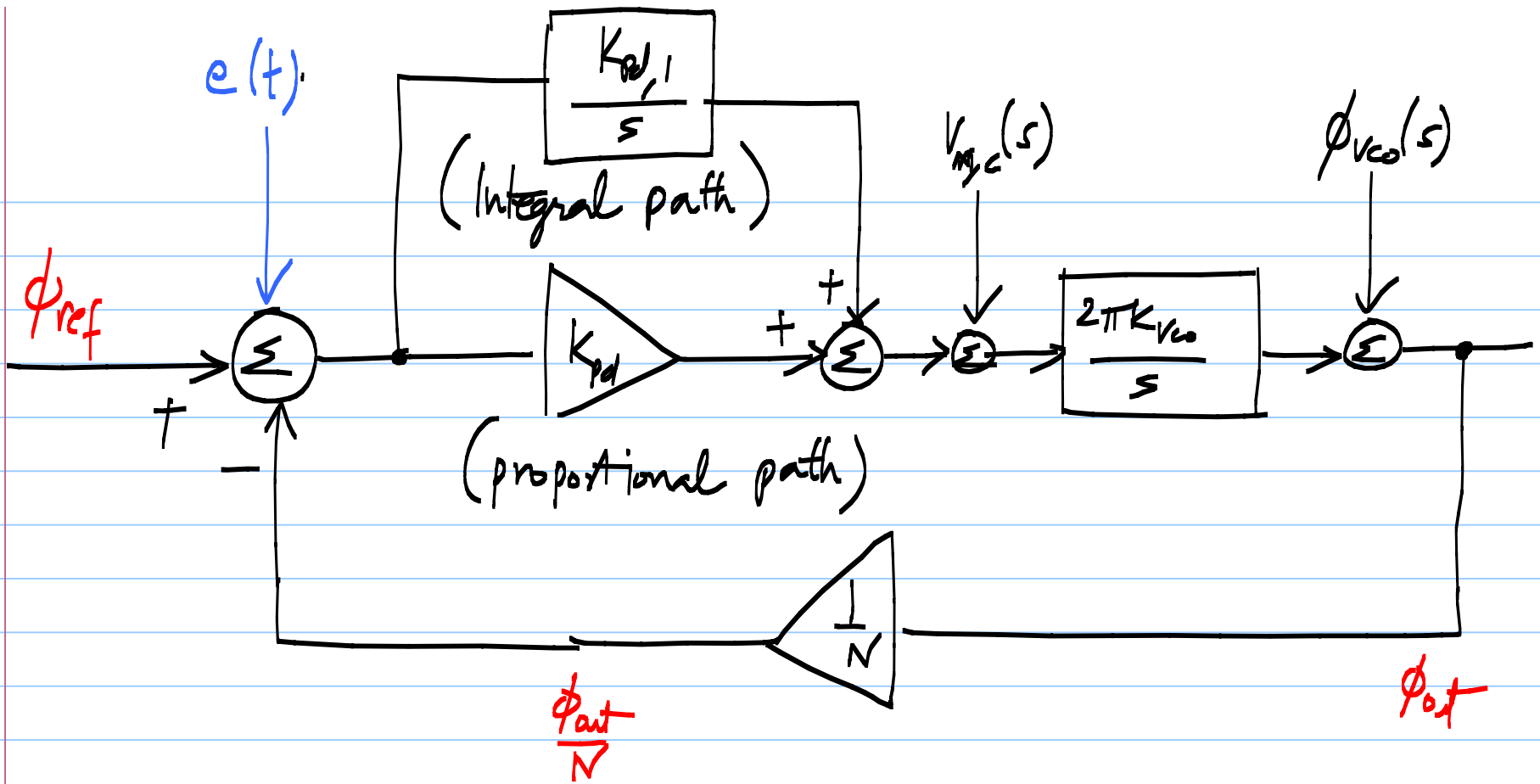


Continuous time approximation valid

$$\text{if } f_{ref} \gg f_{BW} = \frac{K_{pd} K_{v\omega}}{N}$$

(Hz)

$$\underline{f_{ref} \geq 10 \cdot \frac{K_{pd} K_{v\omega}}{N}}$$



$$\frac{\phi_{out}(s)}{\phi_{ref}(s)}$$

$$\phi_{ref}(s)$$

$$\frac{\phi_{out}(s)}{V_e(s)}$$

$$V_e(s)$$

$$\frac{\phi_{out}(s)}{\phi_{vco}(s)}$$

$$\phi_{vco}(s)$$

$$\frac{\phi_{out}(s)}{V_e(s)} = \frac{2\pi K_{vco}}{s}$$

$$\frac{2\pi K_{vco}}{s}$$

$$\frac{\phi_{out}(s)}{\phi_{vco}(s)} = \frac{1}{1+L(s)}$$

$$\frac{1}{1+L(s)}$$

$$\frac{\phi_{out}(s)}{\phi_{ref}(s)} = \frac{\left(\frac{K_{pd,1}}{s} + K_{pd}\right) \frac{2\pi K_{vco}}{s}}{1+L(s)}$$