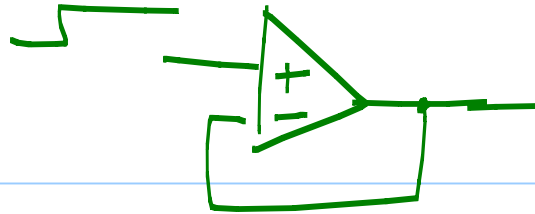


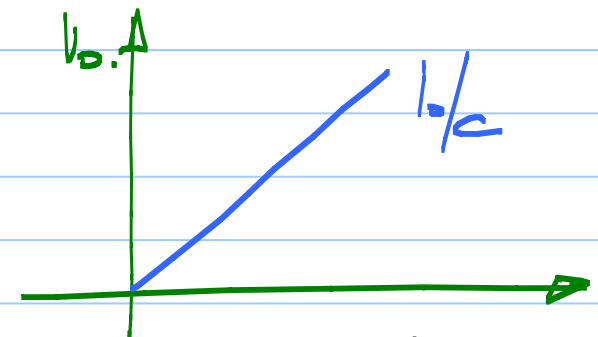
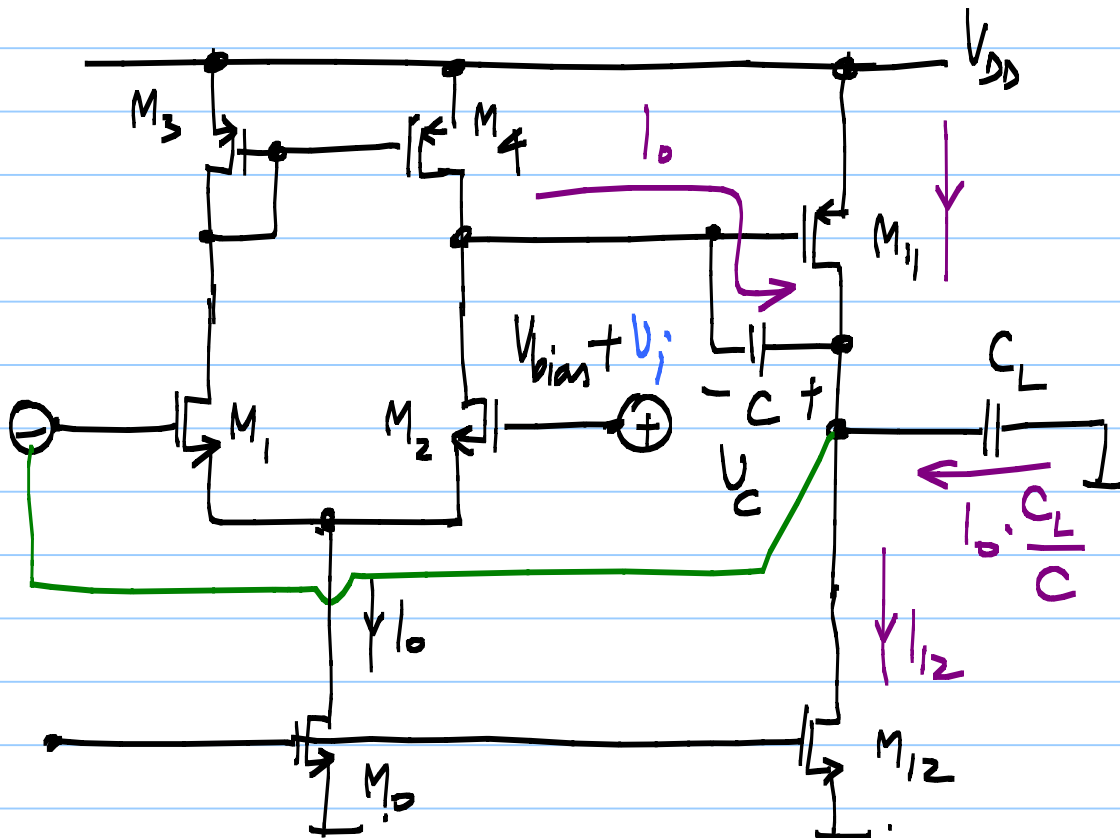
Lecture 37:



Slew rate:

Rate of change of
Voltage across C

$$(V_c) = \pm \frac{I_0}{C}$$



$$I_{D11} = I_{12} - I_0 \left(1 + \frac{C_L}{C}\right)$$

$$I_{D11} = I_{12} - I_0 \left(1 + \frac{C_L}{C}\right) > 0$$

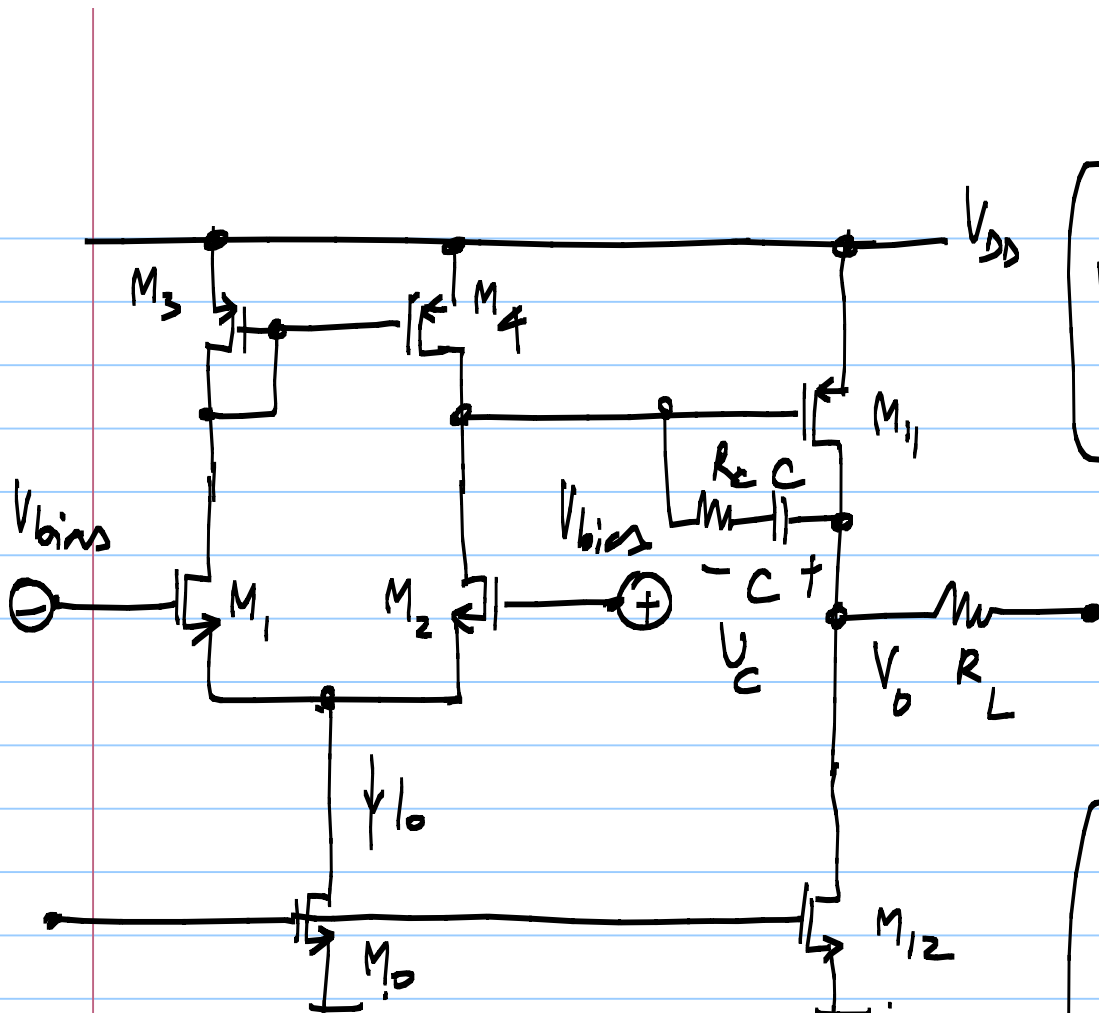
If $I_{12} > I_0 \left(1 + \frac{C_L}{C}\right)$; output will reduce
@ $\frac{I_0}{C}$

$$I_{12} < I_0 \left(1 + \frac{C_L}{C}\right) ?$$

$$\left. \begin{array}{l} \text{output slew rate} = \frac{I_{12}}{C_L + C} \end{array} \right\} \begin{array}{l} \text{Total current} \\ \text{in } C \text{ \& } C_L \\ = I_{12} \end{array}$$

$$SR_+ = \frac{I_0}{C}$$

$$SR_- = \min \left[\frac{I_0}{C}, \frac{I_{12}}{C_L + C} \right]$$



$$V_{T_1} + V_{DSAT_1} < V_{bias} < V_{DD} - V_{SG3} + V_{T_1} + V_{DSAT_0}$$

$$V_{DSAT_{1,2}} < V_0 < V_{DD} - V_{DSAT_{11}}$$

R_C in series with C to cancel the RHP zero

Two stage opamp:

$$A_0 = \frac{g_{m1}}{g_{ds1} + g_{ds3}} \cdot \frac{g_{m11}}{g_{ds11} + g_{ds12} + g_L}$$

$$H(s) = A_0 \left(\frac{1 + s \frac{C_{D3}}{2g_{m3}}}{1 + s \frac{C_{D3}}{g_{m3}}} \right) \cdot \frac{1 - s/z_1}{\left(1 + \frac{s}{P_1}\right) \left(1 + \frac{s}{P_2}\right)}$$

$$S_{V_{in}} = \frac{16}{3} \cdot \frac{kT}{g_{m1}} \left(1 + \frac{g_{m3}}{g_{m1}}\right)$$

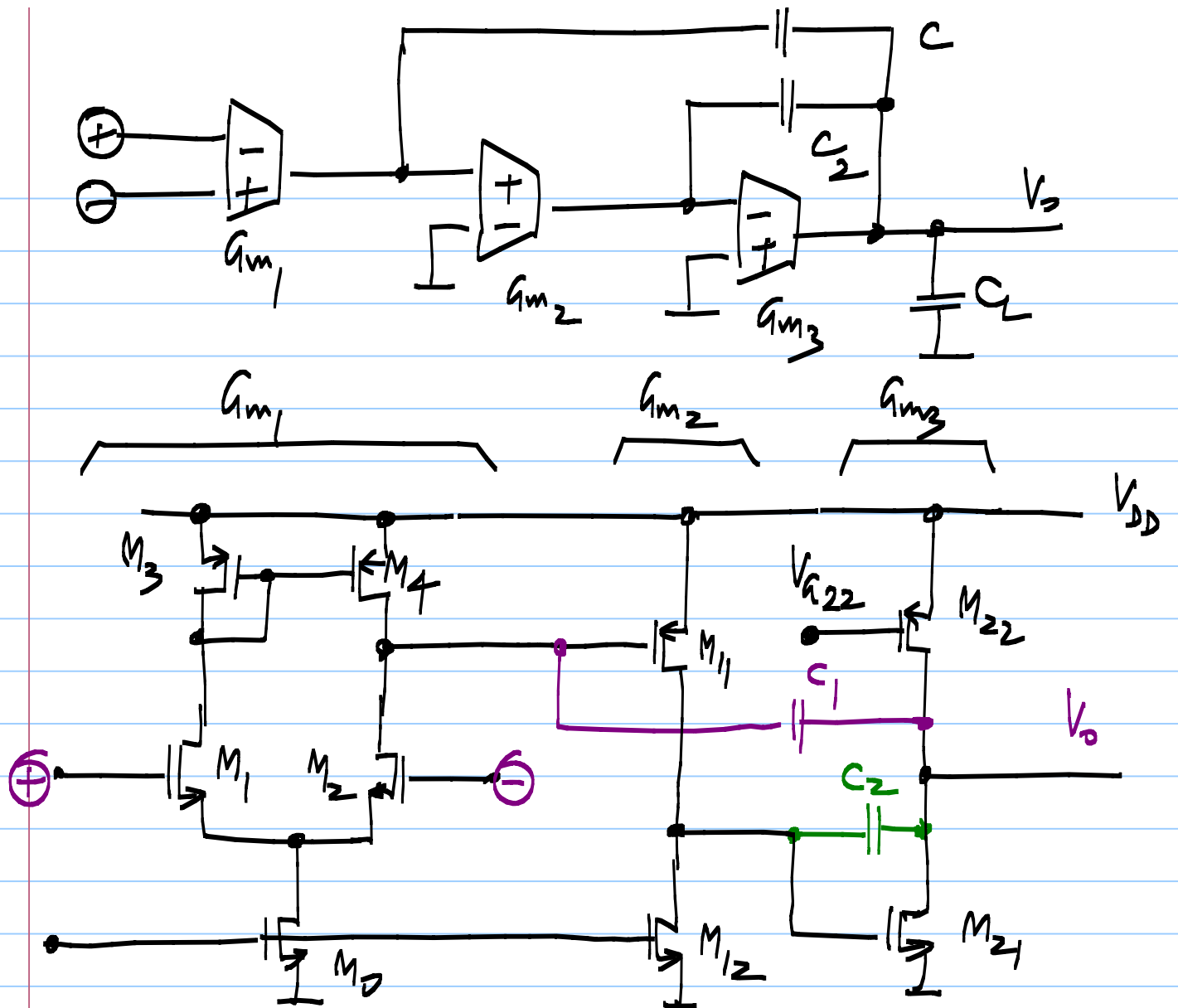
$$\sigma_{V_{os}}^2 = \sigma_{V_{1,12}}^2 + \left(\frac{g_{m3}}{g_{m1}}\right)^2 \sigma_{V_{1,34}}^2$$

$$SR_+ = I_0 / C$$

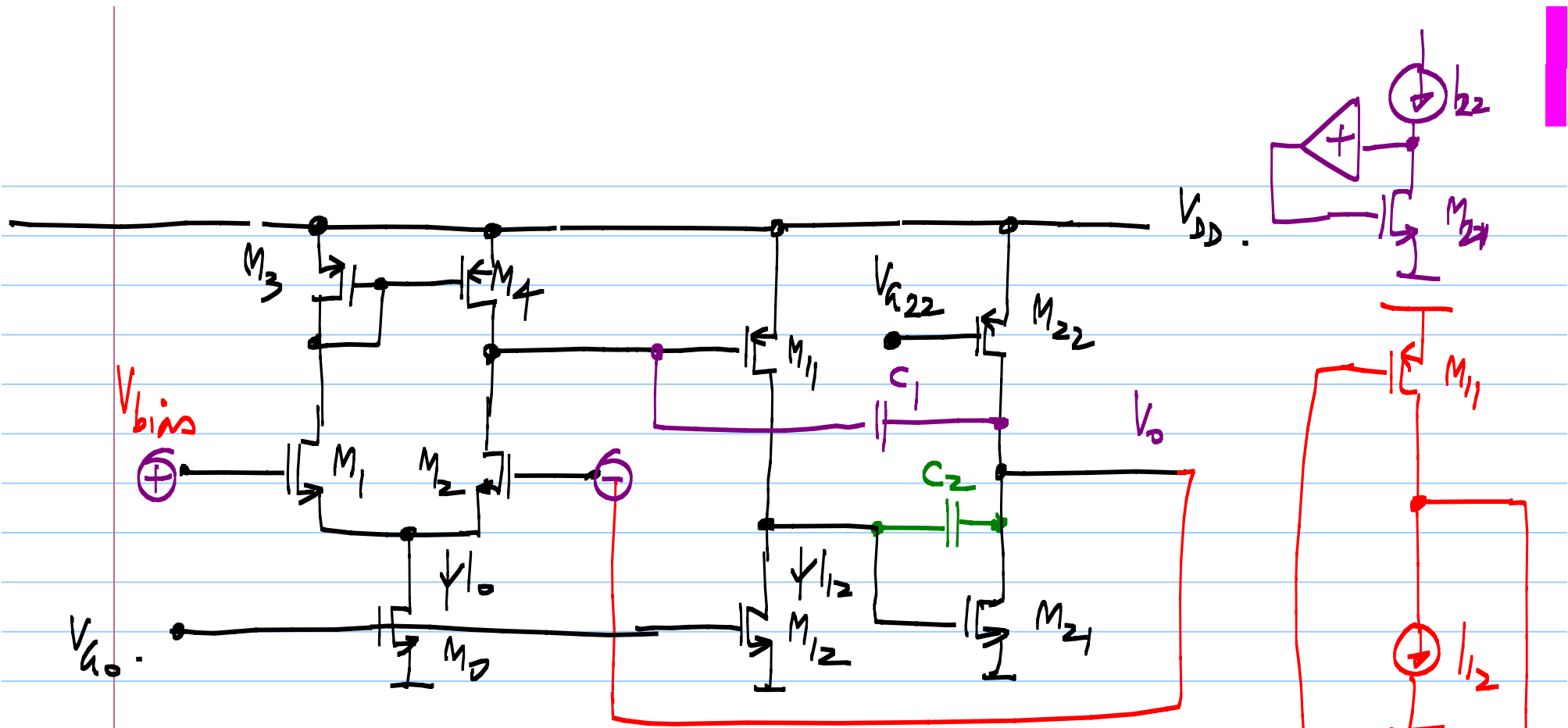
$$SR_- = \min\left(\frac{I_0}{C}, \frac{I_{12}}{C_L + C}\right)$$

$$V_{T1} + V_{DSAT0} < V_{bias} < V_{DD} - V_{SG3} + V_{T1} + V_{DSAT1}$$

$$V_{DSAT1,2} < V_{out} < V_{DD} - V_{DSAT1}$$

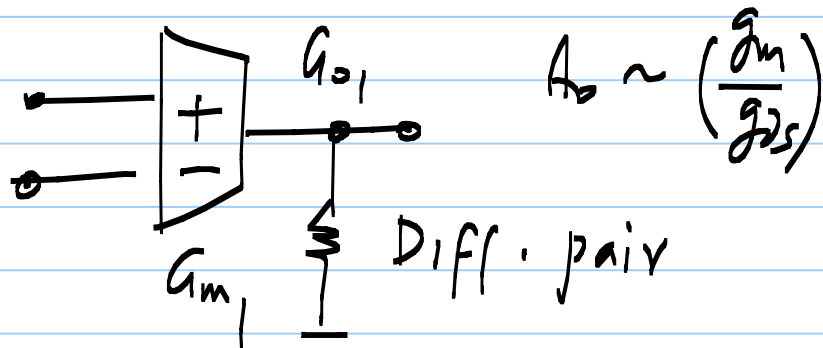


Three
stage
nested
Miller
compensated
opamp

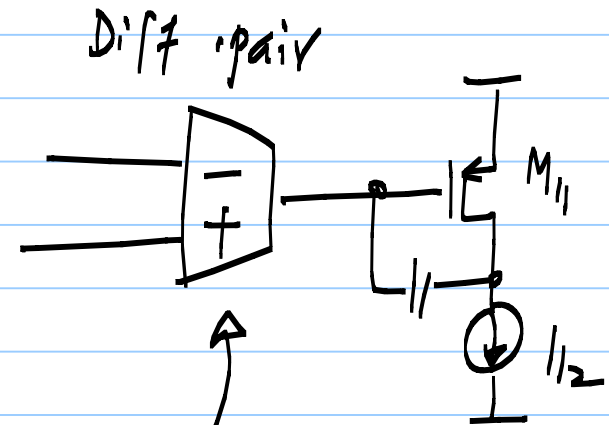


$$\frac{I_0}{W_0} = \frac{I_{12}}{W_{12}} = \frac{I_0'}{W_0'} ; \quad \underline{L_0' = L_0 = L_{12}}$$

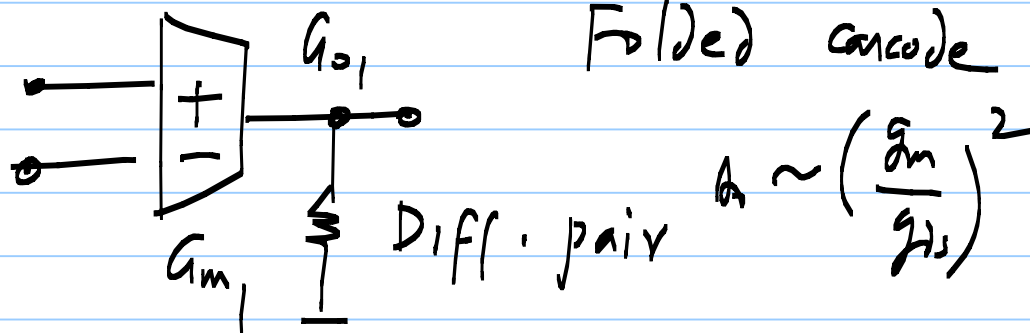
Single stage opamp



Two stage opamp



Telescopic/
Folded cascode



$$\left(\frac{g_m}{g_{D_S}} \right)^2 \left(\frac{g_{m_{11}}}{g_{D_{S_{11}}} + g_{D_{S_{12}}} + g_{12}} \right)$$

