

OP amp data sheet:

* dc gain; dc v_o vs. v_e ; saturation voltages
(V_+ , V_-)

* ac magnitude response $\{ |A(j\omega)|, \angle A(j\omega) \}$

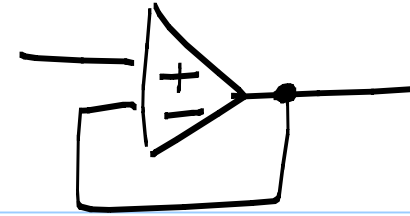
* slew rate

* offset & noise voltages

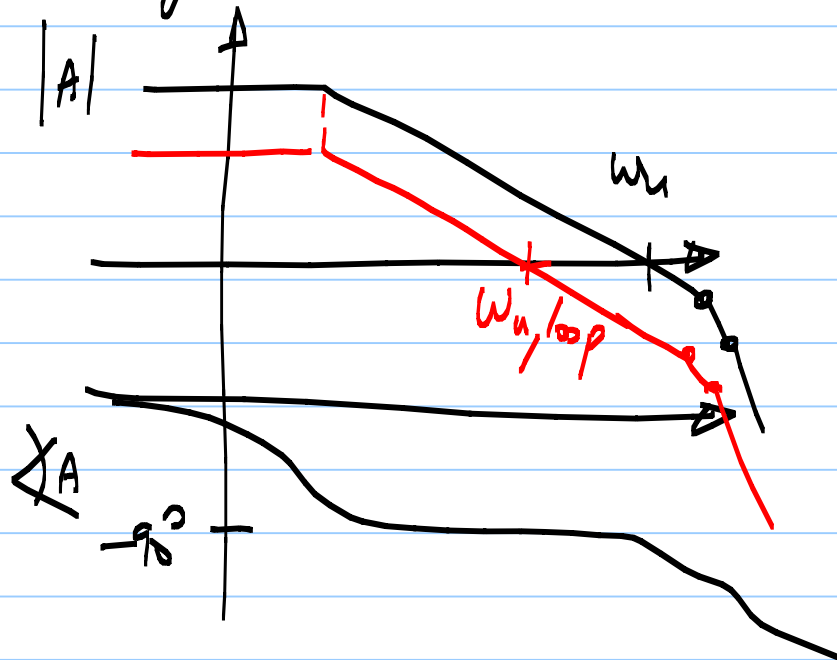
Dominant pole
compensated opamps

* Maximum supply voltage; Maximum load current

Unity gain compensated:



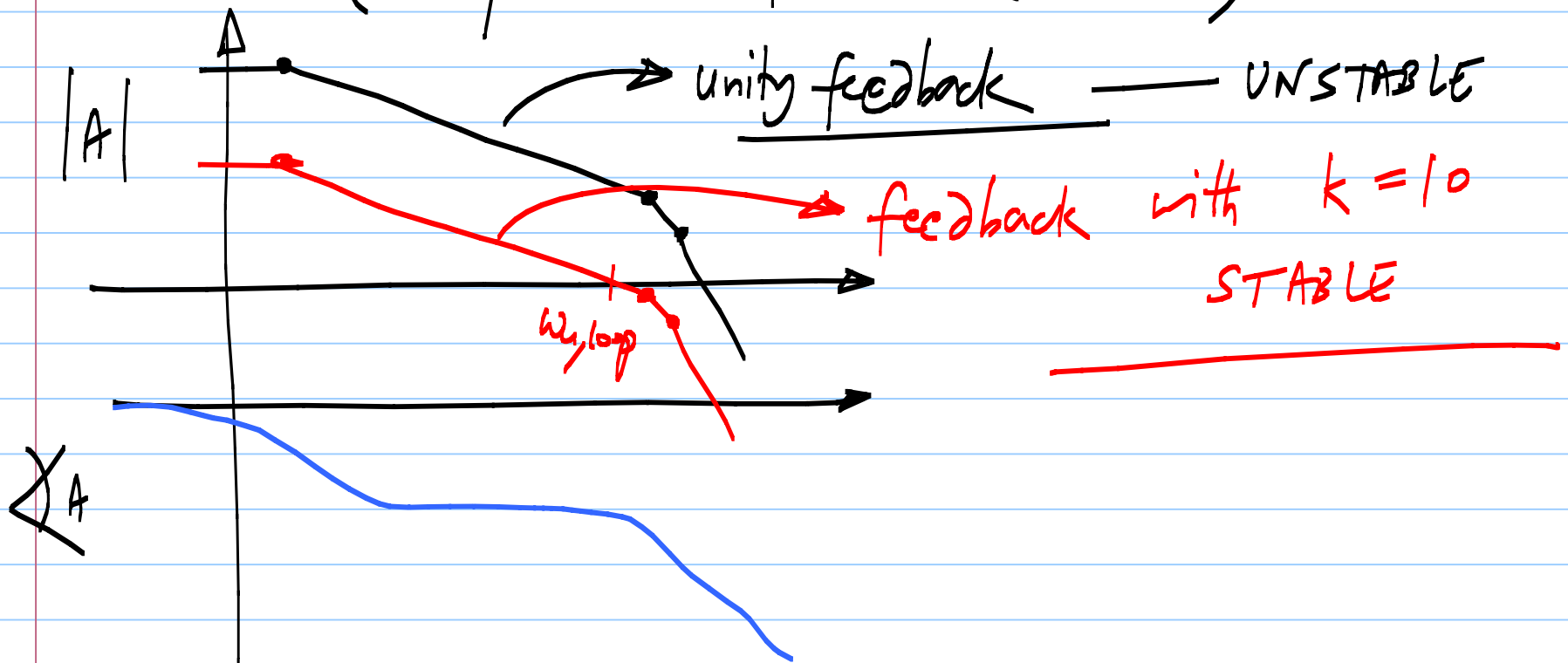
* If the opamp is connected in unity negative feedback, it will be stable.

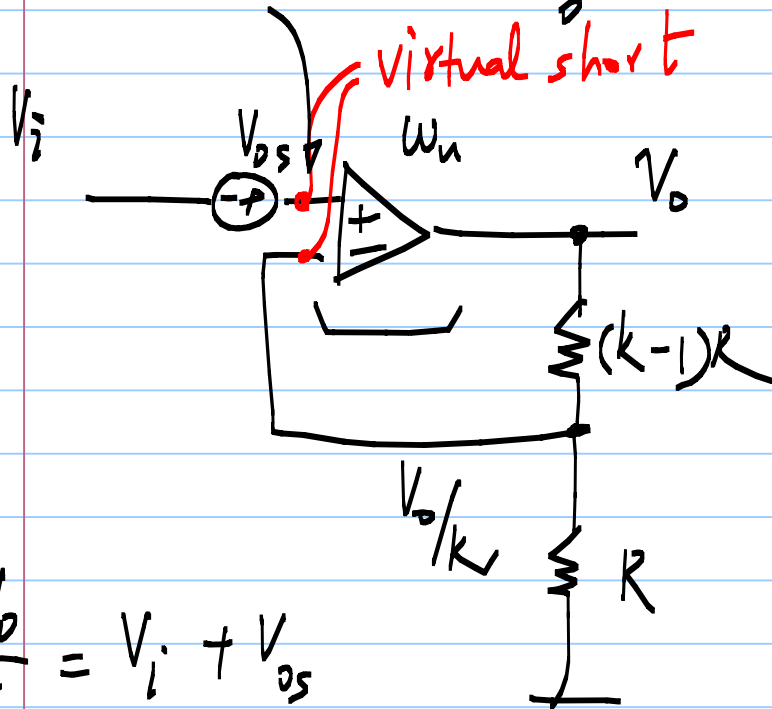
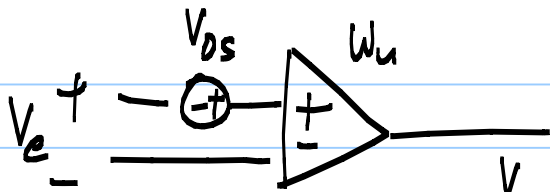


* For any gain $k > 1$ stability is guaranteed.

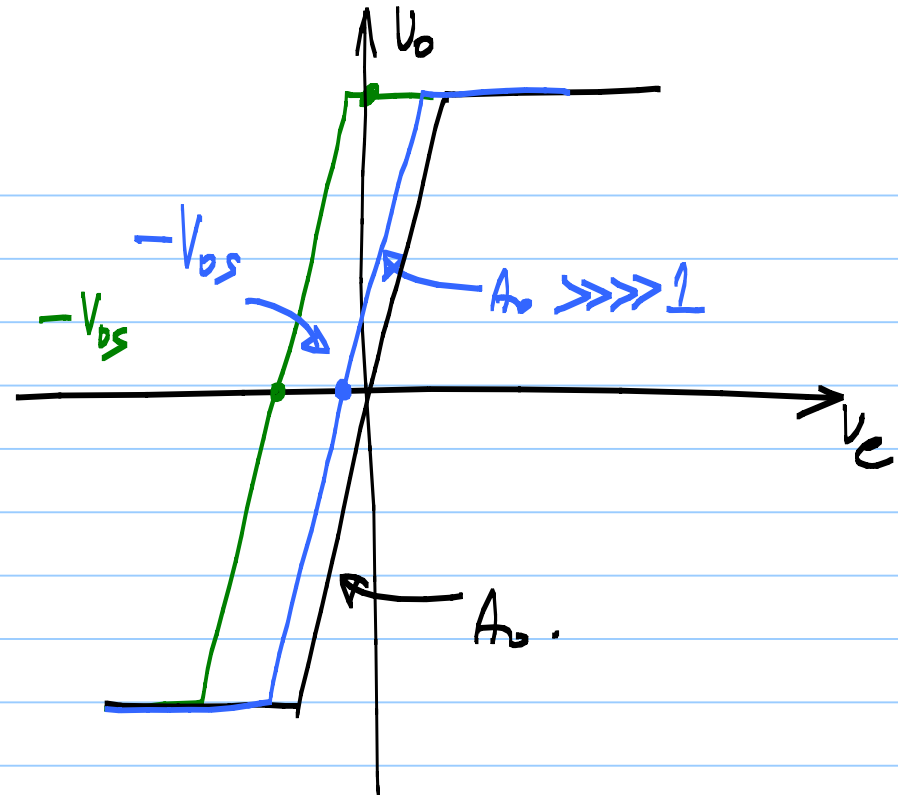
opamps not unity gain compensated; e.g. OPA657

(Compensated for $k > 10$)



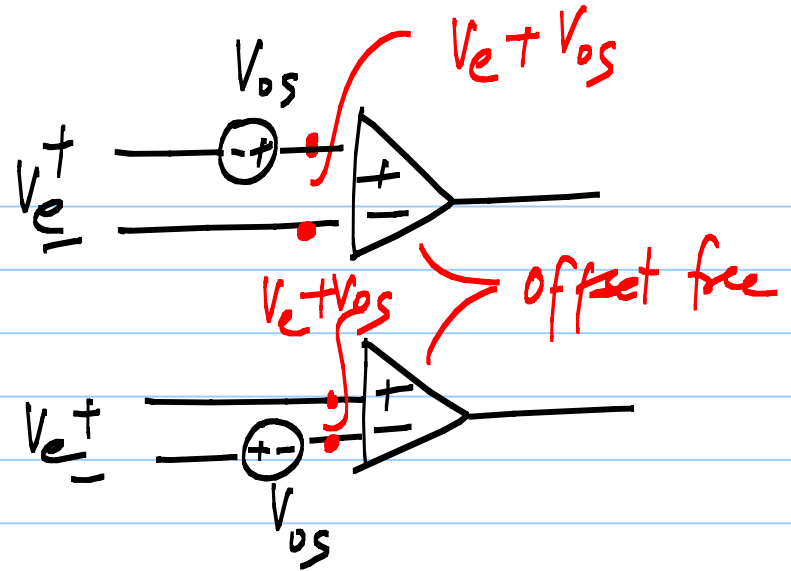
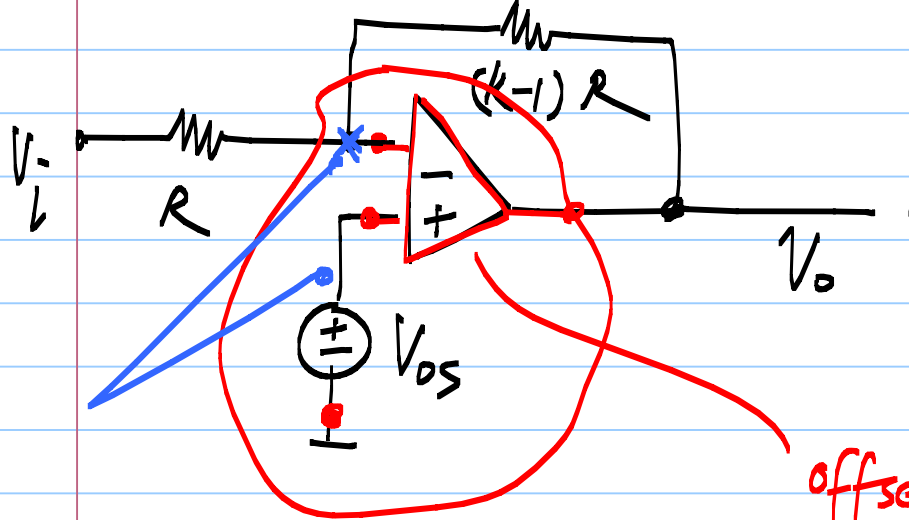


$$\frac{V_0}{k} = V_i + V_{0S}$$



$$V_0 = k V_i + k \cdot V_{0S}$$

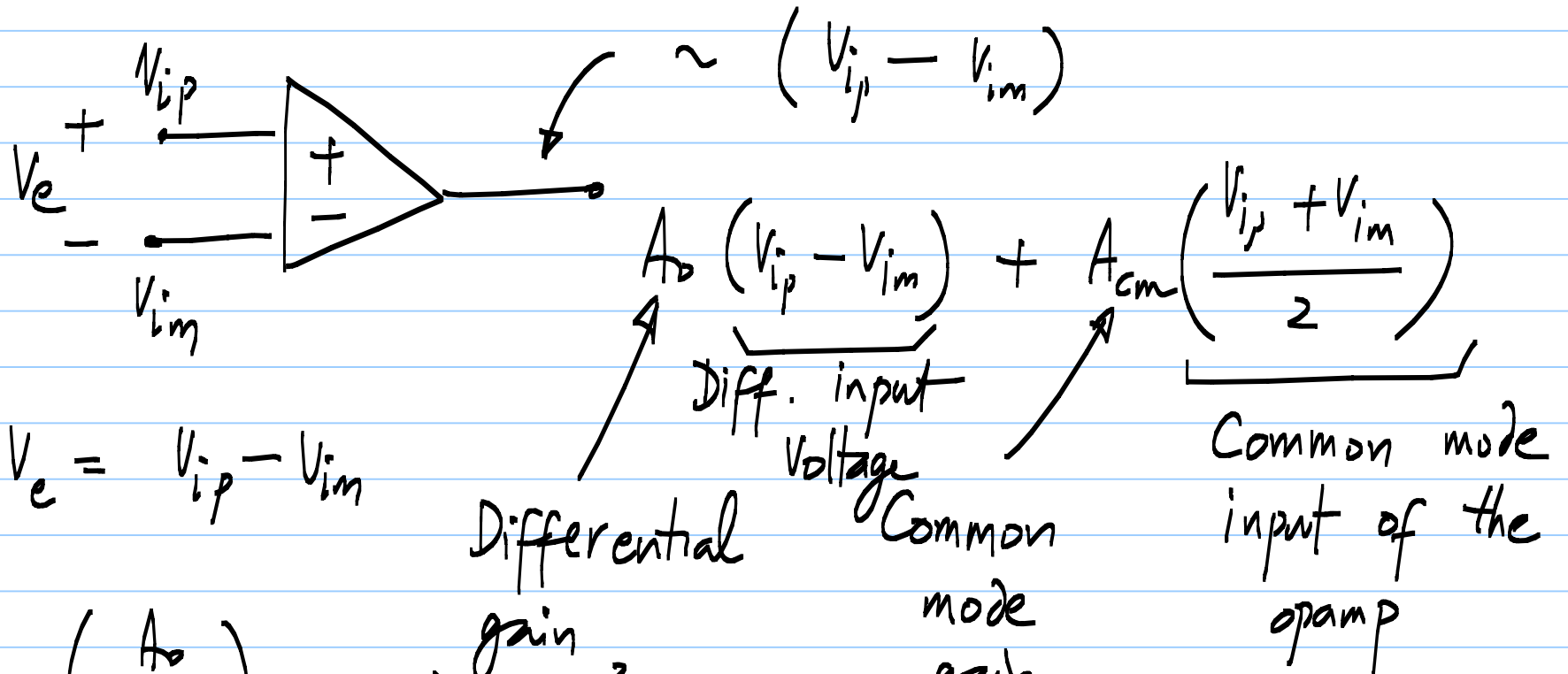
Inverting amplifier;



$$V_i \cdot \frac{k-1}{k} + V_o \cdot \frac{1}{k} = V_{os}$$

$$V_o = - (k-1) V_i + k \cdot V_{os}$$

Common mode gain — Common mode rejection ratio

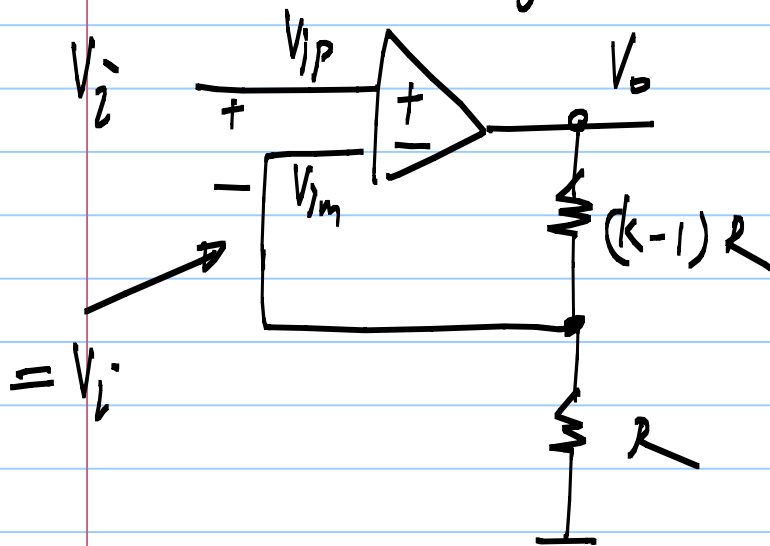


$$20 \log_{10} \left(\frac{A_d}{A_{cm}} \right) = 20 \log_{10} \left(\frac{10^3}{0.1} \right) = \underline{\underline{80 \text{ dB}}}$$

Effect of non-zero common mode gain A_{cm}

Non inverting amp:

Differential gain is very large



$$V_{ip} = V_i, \quad V_{im} = V_i; \quad V_o = kV_i$$

$$V_o = \underbrace{kV_i}_{\text{Ideal}} + \boxed{A_{cm}V_i}$$

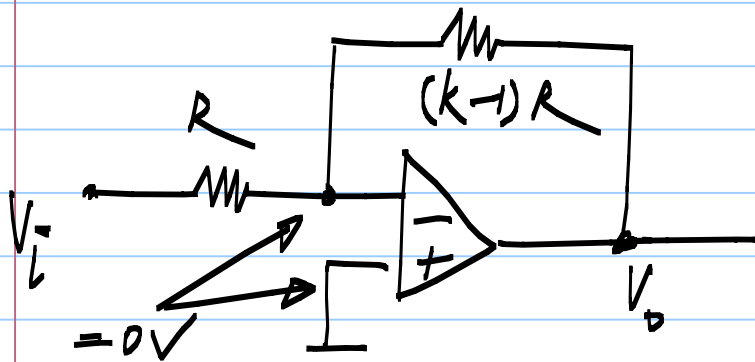
$\left. \begin{array}{l} \text{Non-linearly} \\ \text{related to} \end{array} \right\} V_i$

$$V_o = A_d (V_{ip} - V_{im}) + A_{cm} \left(\frac{V_{ip} + V_{im}}{2} \right)$$

$$V_{im} = \frac{V_o}{k}; \quad V_{ip} = V_i$$

Calculate V_o

Inverting amplifier:



$$A_o \rightarrow \infty$$

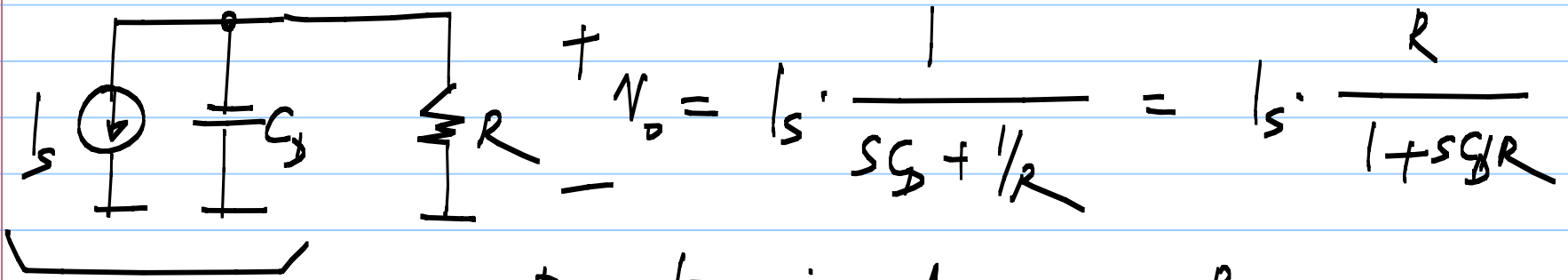
$$\frac{V_{ip} + V_{im}}{2} = 0$$

\approx zero common mode input
for the opamp.

$$V_o = \underbrace{-(k-1)V_i}_{\text{Ideal}} + \underbrace{A_{cm} \cdot 0}_{\text{Error due to } A_{cm}}$$

Transimpedance amplifier:

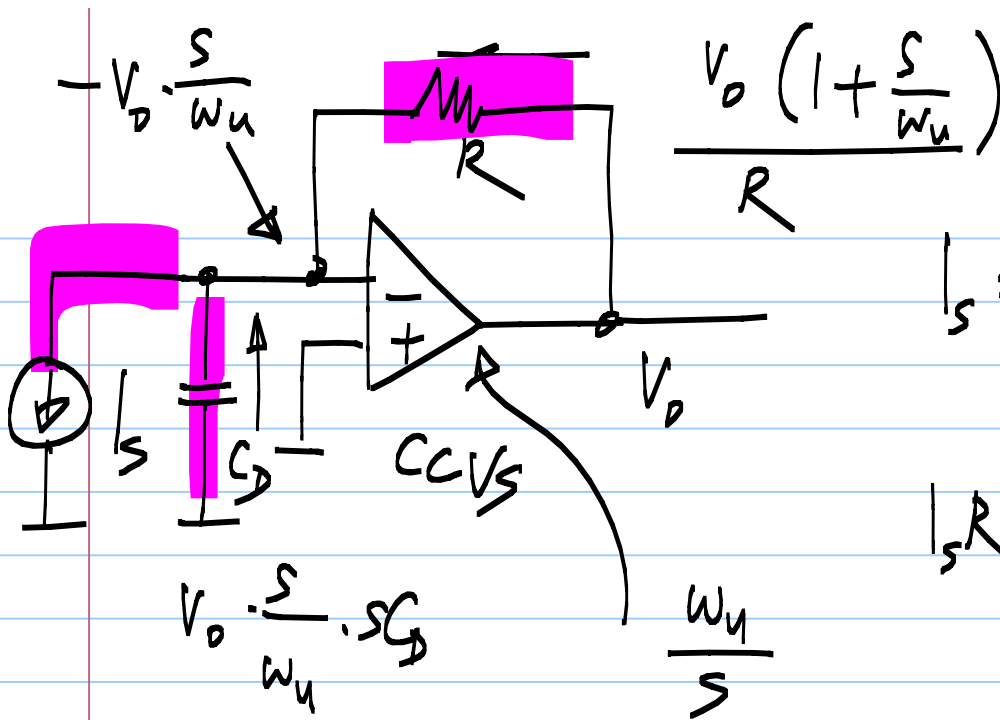
Photodiode:



DC transimpedance : R

Bandwidth : $\frac{1}{C_s R} > \omega_{BW}$

For a given bandwidth : R is fixed. $R < \frac{1}{C_s \omega_{BW}}$



$$I_s = \frac{V_o}{R} \left(1 + \frac{s}{\omega_u}\right) + V_o \cdot \frac{s}{\omega_u} \cdot s C_D$$

$$I_s R = V_o \left(1 + \frac{s}{\omega_u} + \frac{s^2 C_D R}{\omega_u}\right)$$

$$\omega_n = \sqrt{\frac{\omega_u}{C_D R}}$$

$$\frac{V_o}{I_s} = \frac{R}{1 + \frac{s}{\omega_u} + \frac{s^2 C_D R}{\omega_u}}$$

$$1 + 2\zeta \frac{s}{\omega_n} + \frac{s^2}{\omega_n^2}$$

$$\frac{2\zeta}{\omega_n} = \frac{1}{\omega_u} \quad \zeta = \frac{1}{2} \frac{\omega_n}{\omega_u}$$

$$= \frac{1}{2} \sqrt{\frac{1}{\omega_u C_D R}}$$

Damping factor: ζ ; Quality factor: Q

$$\zeta = \frac{1}{2Q} ; \quad Q = \frac{1}{2\zeta}$$

Underdamped system : $\zeta < 1 ; \quad Q > \frac{1}{2}$

Critically damped : $\zeta = 1 ; \quad Q = \frac{1}{2}$

Overdamped system : $\zeta > 1 ; \quad Q < \frac{1}{2}$

$$\frac{V_o}{I_s} = \frac{R}{1 + \frac{s}{\omega_n} + \frac{s^2 GR}{\omega_n}}$$

dc gain: R

$$\omega_n = \sqrt{\frac{\omega_n}{GR}}$$

$$\zeta = \frac{1}{\sqrt{2}} ; \quad \frac{1}{2} \sqrt{\frac{1}{\omega_n GR}} = \frac{1}{\sqrt{2}}$$

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$$\omega_n GR = \frac{1}{2} ; \quad \omega_n = \frac{1}{2GR}$$

$$\omega_n = \sqrt{\frac{1}{2GR} \cdot \frac{1}{GR}} = \frac{1}{\sqrt{2} GR}$$

$$\frac{V_o}{I_s} = \frac{R}{1 + \frac{s}{\omega_n} + \frac{s^2 GR}{\omega_n}}$$

dc gain: R

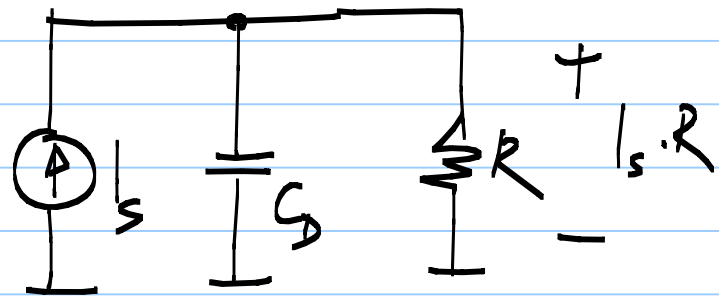
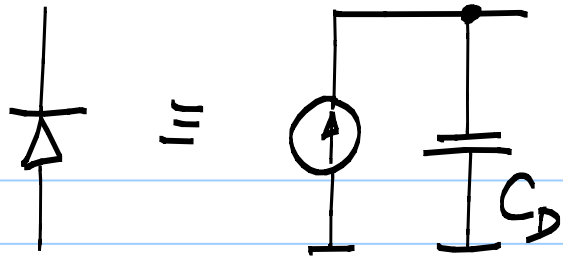
$$\omega_n = \sqrt{\frac{\omega_n}{GR}}$$

$$\zeta = \frac{1}{\sqrt{2}} ; \quad \frac{1}{2} \sqrt{\frac{1}{\omega_n GR}} = \frac{1}{\sqrt{2}}$$

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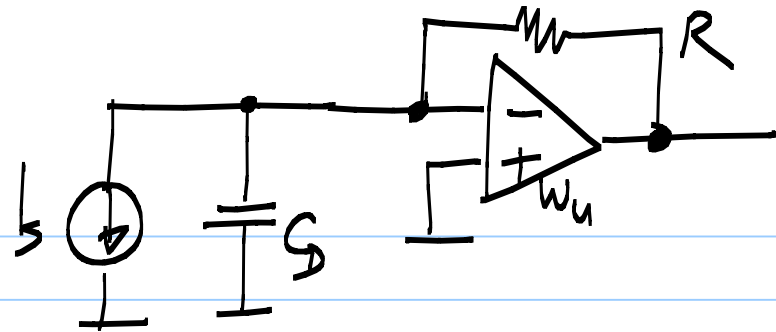
$$\omega_n GR = \frac{1}{2} ; \quad \omega_n = \frac{1}{2GR}$$

$$\omega_n = \sqrt{\frac{1}{2GR} \cdot \frac{1}{GR}} = \frac{1}{\sqrt{2} GR}$$



DC Gain : $\cdot R$

BW : $\frac{1}{C \cdot R}$

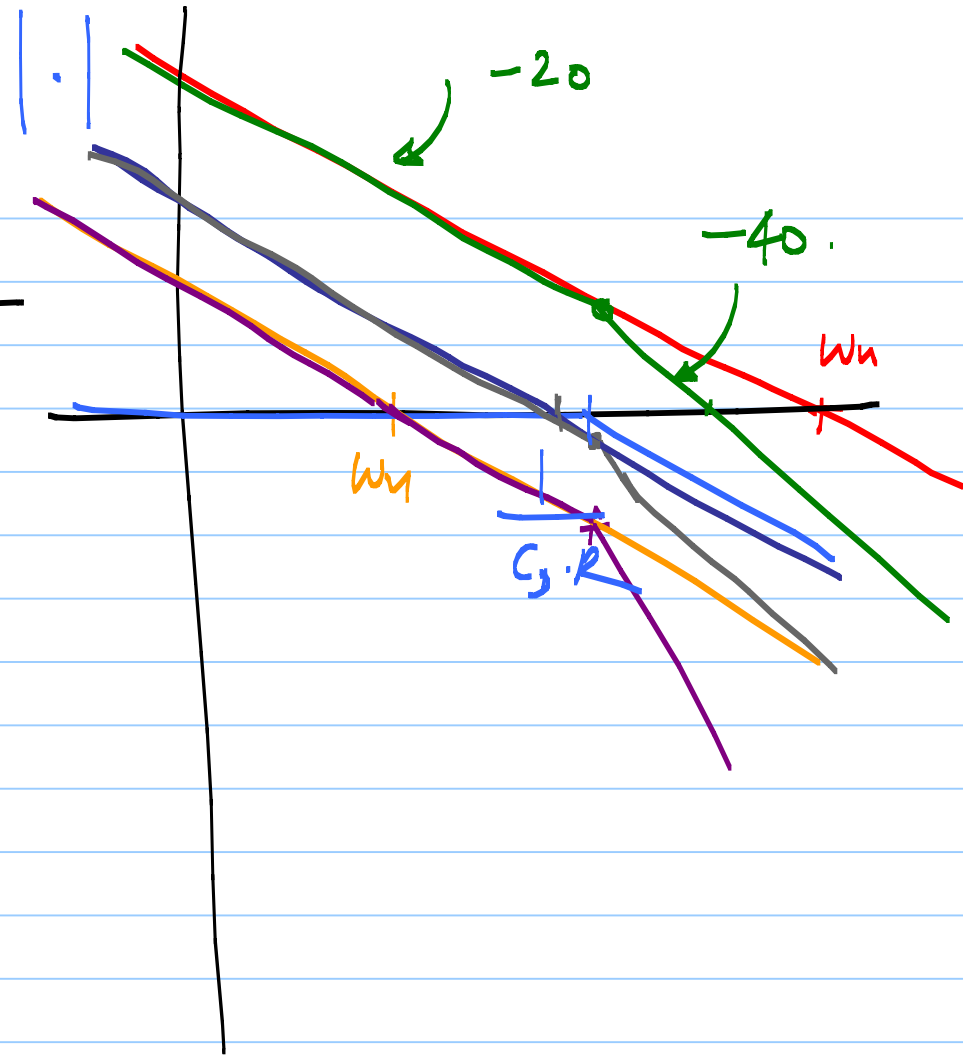
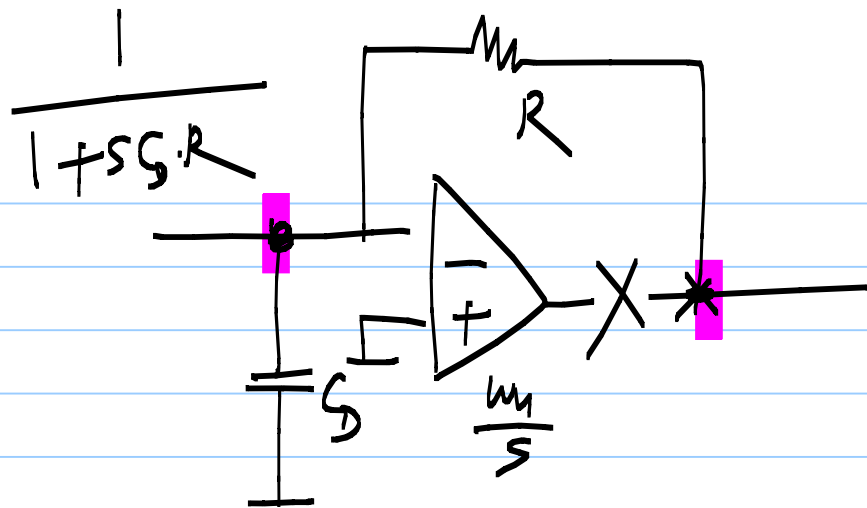


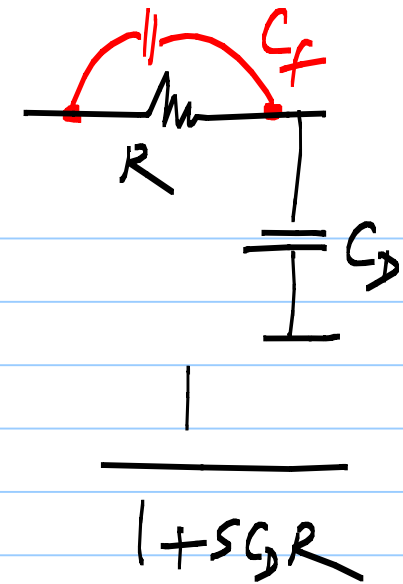
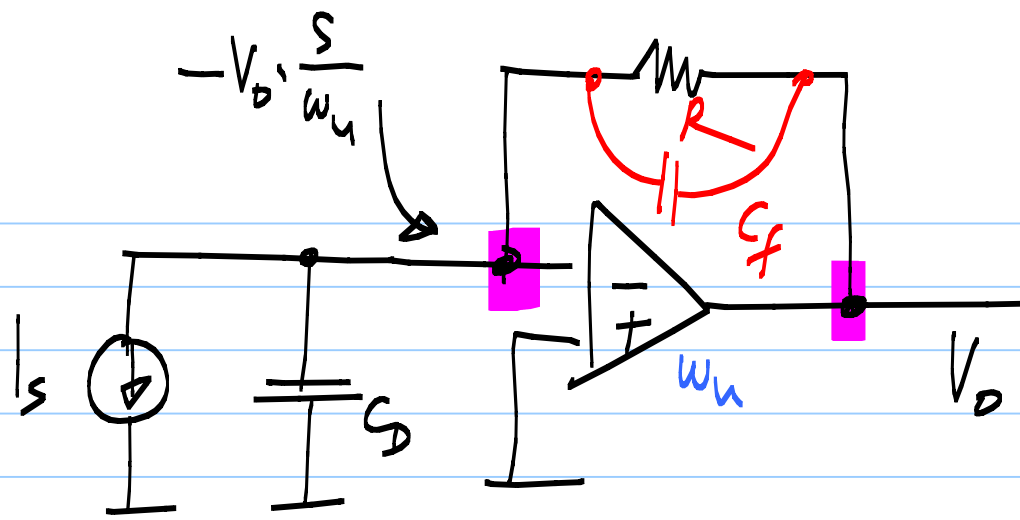
DC gain: R

BW: $\frac{1}{\sqrt{2} C \cdot R}$

$w_u = \frac{1}{2 \cdot C \cdot R}$

$\xi = 1/\sqrt{2}$
 $\Rightarrow \omega = \omega_n$





$$-V_o \cdot \frac{s}{\omega_u} (s C_f + \frac{1}{R_f} + s C_s) - V_o (s C_f + \frac{1}{R_f}) = I_s$$

$$\frac{V_o}{I_s} = \frac{R_f}{s^2 (C_s + C_f) R_f + s \left(\frac{1}{\omega_u} + C_f R_f \right) + 1}$$

$$\frac{1 + s C_f R}{1 + s (C_f + C_s) R}$$

$$\omega_n = \sqrt{\frac{\omega_u}{(G + G_f)R}}$$

$$\sum = \frac{1}{\sqrt{2}}$$

$$\omega_{-3dB} = \omega_n$$

$$\frac{2 \cdot \sum}{\omega_n} = \frac{1}{\omega_u} + G_f \cdot R$$

$$\left\{ (G_f R)^2 = \frac{2 \cdot G_f R \omega_n - 1}{\omega_n^2} \right\}$$

$$\sqrt{2} \cdot \sqrt{\frac{(G + G_f)R}{\omega_n}} = \frac{1}{\omega_u} + G_f R$$

$$2 \cdot \frac{(G + \cancel{G_f})R}{\omega_u} = \frac{1}{\omega_u^2} + \frac{2 \cdot \cancel{G_f}R}{\omega_u} + (G_f R)^2$$

$$\omega_{-3dB} = \omega_n \quad (G_f \cdot R)^2 = \frac{2G_D \cdot R \cdot \omega_n - 1}{\omega_n^2}$$

$$= \sqrt{\frac{\omega_n}{G \cdot R + G_f \cdot R}}$$

$$= \sqrt{\frac{\omega_n}{G \cdot R + \frac{\sqrt{2G_D R \omega_n - 1}}{\omega_n}}} = \sqrt{\frac{\omega_n}{\omega_n \cdot G \cdot R + \sqrt{2G_D R \omega_n - 1}}}$$

$$\omega_{-3dB} = \sqrt{\frac{\omega_n}{\omega_n \cdot G \cdot R + \sqrt{2G_D R \omega_n - 1}}}$$

