

# FREQUENTLY ASKED QUESTIONS (FAQS)

## MODULE 2: STAPLE-FIBRE BASED PROCESSES

**Q12: Define the term intensity of opening?**

A12: The term intensity of opening is defined by the following expression

$$I_{O[\text{mg}]} = \frac{10^6}{60} \frac{P_{[\text{kg}\cdot\text{h}^{-1}]}}{n_{[\text{min}^{-1}]} A_{[\text{cm}^2]} \eta_{[\text{cm}^{-2}]}}$$

where  $I_o$ ...intensity of opening of the opener,  $P$ ...rate of production of the opener,  $n$ ...angular speed of the opener,  $A$ ...surface area of the opener, and  $\eta$ ...number of spikes or teeth density on the opener.

**Q13: It is known that higher air flow rate is required to process fibres with higher aspect ratio in air-lay process. Justify.**

A13: The volumetric flow rate of air required to flow all fibres can be expressed as follows

$$V_0_{[\text{m}^3\cdot\text{h}^{-1}]} = 1.5 \pi l_{[\text{mm}]}^2 \frac{P_{[\text{kg}\cdot\text{h}^{-1}]}}{t_{[\text{den}]}}$$

where  $V_0$  is the volumetric flow rate of air,  $l$  is fibre length,  $P$  is the production rate, and  $t$  is fibre fineness. The fibre fineness can be expressed as

$$t_{[\text{den}]} = \frac{9\pi d_{[\text{mm}]}^2 \rho_{[\text{kg}\cdot\text{m}^{-3}]}}{4}$$

where  $t$  is fibre fineness,  $d$  is fibre diameter, and  $\rho$  is fibre density. By substitution, we obtain

$$V_0_{[\text{m}^3\cdot\text{h}^{-1}]} = \frac{2}{3} \left( \frac{l_{[\text{mm}]}}{d_{[\text{mm}]}} \right)^2 \frac{P_{[\text{kg}\cdot\text{h}^{-1}]}}{\rho_{[\text{kg}\cdot\text{m}^{-3}]}}$$

where  $l/d$  is known as aspect ratio. It is thus clear that higher air flow rate is required to process fibres with higher aspect ratio.

Q14: A carded web of  $25 \text{ g.m}^{-2}$  basis weight and 2.4 m width is fed to a cross-lapper at a feed rate of  $110 \text{ m.min}^{-1}$ . If the desired basis weight of cross-laid batt is  $400 \text{ g.m}^{-2}$  and width of cross-laid batt is 3.8 m then what should be the rate of take-off of cross-laid batt?

A14: It is known that

Basis weight of cross-laid batt = Basis weight of carded web  $\times$  no. of layers

Here, Basis weight of carded web =  $25 \text{ g.m}^{-2}$ ; Desired basis weight of cross-laid batt =  $400 \text{ g.m}^{-2}$ ;  
and No. of layers desired = 16

Further it is known that

Production rate of cross-lapper = Rate of feed of card web  $\times$  width of card web  $\times$  basis weight of card web

Here, Rate of feed of card web =  $110 \text{ m.min}^{-1}$  and Width of card web = 2.4 m

Then, Production rate of cross-lapper =  $(110 \times 2.4 \times 25 \times 60) / 1000 \text{ kg.h}^{-1} = 396 \text{ kg.h}^{-1}$

As it is known that

No. of layers = (width of card web  $\times$  rate of feed of card web) / (width of cross-laid batt  $\times$  rate of take-off of cross-laid batt)

Here, Width of cross-laid batt = 3.8 m

Then

Rate of take-off of cross-laid batt =  $(2.4 \times 110) / (3.8 \times 16) \text{ m.min}^{-1} = 4.34 \text{ m.min}^{-1}$